

# STATE OF CONNECTICUT

## CONNECTICUT SITING COUNCIL

Ten Franklin Square, New Britain, CT 06051

Phone: (860) 827-2935 Fax: (860) 827-2950

E-Mail: [siting.council@ct.gov](mailto:siting.council@ct.gov)

Internet: [ct.gov/csc](http://ct.gov/csc)

Daniel F. Caruso  
Chairman

March 14, 2011

Kenneth C. Baldwin, Esq.  
Robinson & Cole LLP  
280 Trumbull Street  
Hartford, CT 06103-3597

**RE: EM-VER-166-110203B** - Cellco Partnership d/b/a Verizon Wireless notice of intent to modify an existing telecommunications facility located at 1192 Wolcott Road, Wolcott, Connecticut.

Dear Attorney Baldwin:

The Connecticut Siting Council (Council) hereby acknowledges your notice to modify this existing telecommunications facility, pursuant to Section 16-50j-73 of the Regulations of Connecticut State Agencies with the following conditions:

- Any deviation from the proposed modification as specified in this notice and supporting materials with Council shall render this acknowledgement invalid;
- Any material changes to this modification as proposed shall require the filing of a new notice with the Council;
- Not less than 45 days after completion of construction, the Council shall be notified in writing that construction has been completed;
- The validity of this action shall expire one year from the date of this letter; and
- The applicant may file a request for an extension of time beyond the one year deadline provided that such request is submitted to the Council not less than 60 days prior to the expiration;

The proposed modifications including the placement of all necessary equipment and shelters within the tower compound are to be implemented as specified here and in your notice dated February 3, 2011. The modifications are in compliance with the exception criteria in Section 16-50j-72 (b) of the Regulations of Connecticut State Agencies as changes to an existing facility site that would not increase tower height, extend the boundaries of the tower site, increase noise levels at the tower site boundary by six decibels, and increase the total radio frequencies electromagnetic radiation power density measured at the tower site boundary to or above the standard adopted by the State Department of Environmental Protection pursuant to General Statutes § 22a-162. This facility has also been carefully modeled to ensure that radio frequency emissions are conservatively below State and federal standards applicable to the frequencies now used on this tower.

This decision is under the exclusive jurisdiction of the Council. Please be advised that the validity of this action shall expire one year from the date of this letter. Any additional change to this facility will require explicit notice to this agency pursuant to Regulations of Connecticut State Agencies Section 16-50j-73. Such notice shall include all relevant information regarding the proposed change with cumulative worst-case modeling of radio frequency exposure at the closest point of uncontrolled access to the tower base, consistent with Federal Communications Commission, Office of Engineering and Technology, Bulletin 65. Thank you for your attention and cooperation.

Very truly yours,

Linda Roberts  
Executive Director

LR/CDM/laf

c: The Honorable Thomas G. Dunn, Mayor, Town of Wolcott  
David Kalinowski, Zoning Enforcement Officer, Town of Wolcott  
Graziano Tower

# ROBINSON & COLE

EM-VER-166-110203B

KENNETH C. BALDWIN

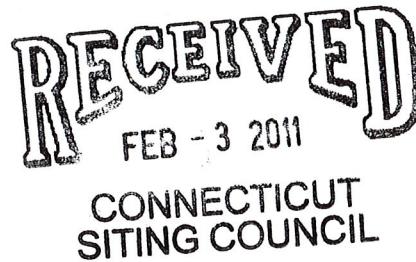
280 Trumbull Street  
Hartford, CT 06103-3597  
Main (860) 275-8200  
Fax (860) 275-8299  
kbaldwin@rc.com  
Direct (860) 275-8345

ORIGINAL

February 3, 2011

*Via Hand Delivery*

Linda Roberts  
Executive Director  
Connecticut Siting Council  
10 Franklin Square  
New Britain, CT 06051



Re: **Notice of Exempt Modification – Antenna Swap  
1192 Wolcott Road, Wolcott, Connecticut**

Dear Ms. Roberts:

Cellco Partnership d/b/a Verizon Wireless (“Cellco”) currently maintains twelve (12) wireless telecommunications antennas at the 135-foot level on the existing 180-foot tower at the above-referenced address. The tower is owned by Graziano Tower, LLC. The Connecticut Siting Council (“Council”) approved Cellco’s use of this tower in 1997. Cellco intends to remove all of its existing antennas and replace them with twelve (12) new antennas (four (4) model APL868013-42T0 cellular antennas; two (2) model APL866513-42T0 cellular antennas; two (2) APX18-206516L-T0 PCS antennas; one (1) model MG D3-800T0 PCS antenna; and three (3) model BXA 70063/6CF LTE antennas). All new antennas will be installed at the same 135-foot level on the tower. Cellco will also install six (6) coax cable diplexers on its existing antenna platform. Attached behind Tab 1 of this filing are the specifications for each of the proposed replacement antennas and cable diplexers.



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Please accept this letter as notification pursuant to R.C.S.A. § 16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to Thomas Dunn, Mayor for the Town of Wolcott. A copy of this letter is also being sent to Graziano Tower, LLC, the owner of the property on which the tower is located.

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2).

# ROBINSON & COLE LLP

Linda Roberts  
February 3, 2011  
Page 2

1. The proposed modifications will not result in any increase in the overall height of the existing tower. Cellco's replacement antennas and diplexers will be located at the 135-foot level on the 180-foot tower.

2. The proposed modifications will not involve any modifications to ground-mounted equipment and, therefore, will not require the extension of the site boundaries.

3. The proposed modifications will not increase noise levels at the facility by six decibels or more.

4. The operation of the replacement antennas will not increase radio frequency (RF) power density levels at the facility to a level at or above the Federal Communications Commission (FCC) adopted safety standard. A cumulative General Power Density table for the modified facility is included behind Tab 2.

Also attached is a Structural Analysis Report confirming that the tower and foundation can support Cellco's proposed modifications. (See Tab 3).

For the foregoing reasons, Cellco respectfully submits that the proposed modifications to the above-referenced telecommunications facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

Sincerely,



Kenneth C. Baldwin

Enclosures  
Copy to:

Thomas Dunn, Wolcott Mayor  
Graziano Tower, LLC  
Sandy M. Carter



## Maximizer® Log Periodic Antenna, 806-894, 80deg, 14.1dBi, 1.2m, FET, 0deg

**Product Description**

The Celwave® Maximizer series is a log periodic dipole array which uses a patented design to achieve a front-to-back ratio of 45 dB, the highest front-to-back ratio in the industry. Maximizers are available to cover ESMR, AMPS, PCS and DCS frequency ranges. They use RFS's patented monolithic CELlite® technology, which eliminates cable and soldered joints to reduce the possibility of inter-modulation products. The CELlite technology assures high reliability and excellent repeatability of electrical characteristics. The cellular Maximizers are available in 65°, 80° and 90° horizontal beamwidths and the PCS/DCS Maximizers are available in 65° and 90° horizontal beamwidths. Patent number 6,133,889.

**Features/Benefits**

- 45 dB front-to-back ratio reduces co-channel interference.
- Monolithic construction reduces IM.
- No solder joints, high reliability.
- Surface treated components prevent galvanic corrosion.
- UV stabilized radome assures long life without radome deterioration due to UV exposure.

**Technical Specifications****Electrical Specifications**

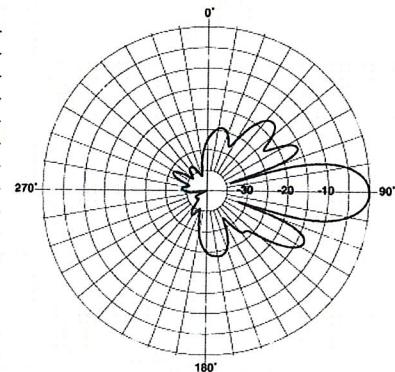
Frequency Range, MHz	806-894
Horizontal Beamwidth, deg	80
Vertical Beamwidth, deg	15
Electrical Downtilt, deg	0
Gain, dBi (dBd)	14.1 (12)
Front-To-Back Ratio, dB	45
Polarization	Vertical
VSWR	< 1.5:1
Impedance, Ohms	50
Maximum Power Input, W	500
Lightning Protection	Direct Ground
Connector Type	7-16 DIN Female

**Mechanical Specifications**

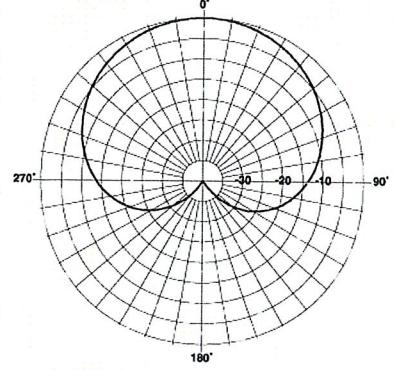
Dimensions - HxWxD, mm (in)	1219 x 152 x 203 (48 x 6 x 8)
Weight w/o Mtg Hardware, kg (lb)	2.8 (6.32)
Survival Wind Speed, km/h (mph)	200 (125)
Rated Wind Speed, km/h (mph)	200 (125)
Max Wind Loading Area, m² (ft²)	0.307 (3.3)
Maximum Thrust @ Rated Wind, N (lbf)	916 (206)
Wind Load - Side @ Rated Wind, N (lbf)	743 (167)
Radome Material	UV Stabilized High Impact ABS
Shipping Weight, kg (lb)	7.9 (17.5)
Packing Dimensions, HxWxD, mm (in)	1270 x 305 x 203 (50 x 12 x 8)

**Ordering Information**

Mounting Hardware	APM21-3
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Vertical Pattern



Horizontal Pattern

**Other Documentation**

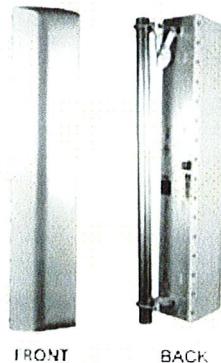
## Maximizer® Log Periodic Antenna, 806-894, 65deg, 15.1dBi, 1.2m, FET, 0deg

## Product Description

The Celwave® Maximizer series is a log periodic dipole array which uses a patented design to achieve a front-to-back ratio of 45 dB, the highest front-to-back ratio in the industry. Maximizers are available to cover ESMR, AMPS, PCS and DCS frequency ranges. They use RFS's patented monolithic CELlite® technology, which eliminates cable and soldered joints to reduce the possibility of inter-modulation products. The CELlite technology assures high reliability and excellent repeatability of electrical characteristics. The cellular Maximizers are available in 65°, 80° and 90° horizontal beamwidths and the PCS/DCS Maximizers are available in 65° and 90° horizontal beamwidths. Patent number 6,133,889.

## Features/Benefits

- 45 dB front-to-back ratio reduces co-channel interference. • Monolithic construction reduces IM.
- No solder joints, high reliability. • Surface treated components prevent galvanic corrosion. • UV stabilized radome assures long life without radome deterioration due to UV exposure.



FRONT

BACK

## Technical Specifications

## Electrical Specifications

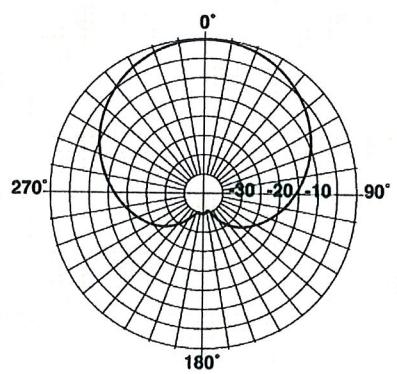
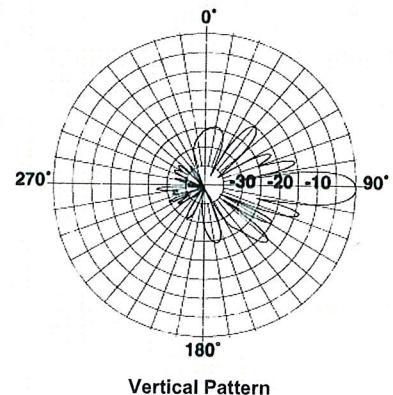
Frequency Range, MHz	806-894
Horizontal Beamwidth, deg	65
Vertical Beamwidth, deg	15
Electrical Downtilt, deg	0
Gain, dBi (dBd)	15.1 (13)
1st Upper Sidelobe Suppression, dB	>20
Upper Sidelobe Suppression, dB	>20
Front-To-Back Ratio, dB	45
Polarization	Vertical
VSWR	< 1.5:1
Impedance, Ohms	50
Maximum Power Input, W	500
Lightning Protection	Direct Ground
Connector Type	7-16 DIN Female

## Mechanical Specifications

Dimensions - HxWxD, mm (in)	1219 x 234 x 203 (48 x 9.2 x 8)
Weight w/o Mtg Hardware, kg (lb)	7 (15.7)
Survival Wind Speed, km/h (mph)	200 (125)
Rated Wind Speed, Km/h (mph)	180 (112)
Max Wind Loading Area, m² (ft²)	0.376 (4.05)
Maximum Thrust @ Rated Wind, N (lbf)	903 (203)
Wind Load - Side @ Rated Wind, N (lbf)	594 (133.5)
Radome Material	UV Stabilized High Impact ABS
Shipping Weight, kg (lb)	9.1 (20)
Packing Dimensions, HxWxD, mm (in)	1594 x 343 x 349 (62.75 x 13.5 x 13.75)

## Ordering Information

Mounting Hardware	APM21-3
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## Other Documentation

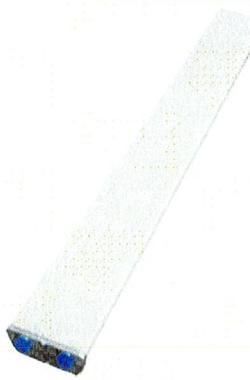
Optimizer® Dual Polarized Antenna, 1710-2170, 65deg, 17.6/18.6dBi, 1.3m, FET, 0deg

**Product Description**

Dense urban networks where site aspect is essential.

**Features/Benefits**

- Very broadband design operating from GSM1800 up to 3G-UMTS.
- Reduction of visual impact by gathering 3 antennas in a cylindrical volume.
- Reduction of site dimensions will ease site acceptance.
- Possible camouflage solution on demand.
- Wind load thrust highly reduced.
- Compatible with usual base stations with 35 dB typical isolation between ports.
- Effective polarization diversity ensured by high cross polar discrimination.
- Optimized suppression of side lobes allows strong mechanical tilt.

**Technical Specifications****Electrical Specifications**

	1710-1900	1900-2170
Horizontal Beamwidth, deg	69	64
Vertical Beamwidth, deg	6.9	6
Electrical Downtilt, deg	0	
Gain, dBi (dBd)	17.6 (15.5)	18.6 (16.5)
1st Upper Sidelobe Suppression, dB	>20	
Front-To-Back Ratio, dB	>29	30
Polarization	Dual pol +/-45°	
VSWR	< 1.4:1	
Isolation between Ports, dB	>30 (typ 35)	
3rd Order IMP @ 2 x 43 dBm, dBc	>150, N/A	
7th Order IMP @ 2 x 46 dBm, dBc	N/A, >170	
Impedance, Ohms	50	
Maximum Power Input, W	300	
Lightning Protection	Direct Ground	
Connector Type	(2) 7-16 Long Neck Female	

**Mechanical Specifications**

Dimensions - HxWxD, mm (in)	1349 x 169 x 80 (53.0 x 6.65 x 3.15)
Weight w/o Mtg Hardware, kg (lb)	8.5 (18.7)
Survival Wind Speed, km/h (mph)	200 (125)
Rated Wind Speed, km/h (mph)	160 (100)
Max Wind Loading Area, m² (ft²)	0.23 (2.46)
Front Thrust @ Rated Wind, N (lbf)	406 (91)
Maximum Thrust @ Rated Wind, N (lbf)	406 (91)
Wind Load - Side @ Rated Wind, N (lbf)	236 (53)
Wind Load - Rear @ Rated Wind, N (lbf)	196 (44)
Radome Material	Fiberglass
Radome Color	Light Grey RAL7035
Mounting Hardware Material	Diecasted Aluminum
Shipping Weight, kg (lb)	13.5 (30)
Packing Dimensions, HxWxD, mm (in)	1464 x 251 x 203 (57.64 x 9.88 x 7.99)

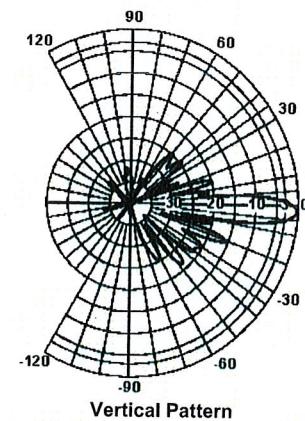
**Ordering Information**

Mounting Hardware	APM40-2
Mounting Pipe Diameter, mm (in)	60-120 (2.36-4.72)
Mounting Hardware Weight, kg (lb)	3.4 (7.5)

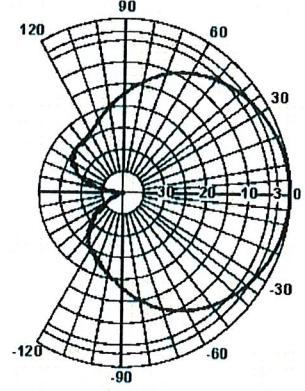
**Other Documentation**

APM40 Series Datasheet

APM40 Series Installation Instructions



Vertical Pattern



Horizontal Pattern



# SINGLE-BAND PANEL ANTENNA

## BROADBAND 1710-2170 MHz

### MGD3-800TX

#### ELECTRICAL SPECIFICATIONS

Antenna Model	MGD3-800TX		
Polarization	$\pm 45^\circ$		
Frequency	1710-2170		
Horizontal Beamwidth	1710 - 1880	1850 - 1990	1920 - 2170
Vertical Beamwidth	66°	64°	63°
Gain (dBi)	7.2°	6.6°	6.3°
Vertical Electrical Tilt	18	18	18.5
Upper Sidelobe Suppression for the 1 <sup>st</sup> lobe above main beam (dB)	0°, 2°, 4°, 6°	0°, 2°, 4°, 6°	0°, 2°, 4°, 6°
Front-to-Back Ratio @ 180° ± 20° (dB)	> 30	> 30	> 30
VSWR	< 1.4 : 1	< 1.4 : 1	< 1.4 : 1
Cross Polar Ratio @ ± 60° (dB)	> 10	> 10	> 10
Isolation between Ports (dB)	> 30	> 30	> 30
Maximum Power Per Input (W)	250		
Intermodulation (dBc)		< - 150	
Impedance ( $\Omega$ )		50	

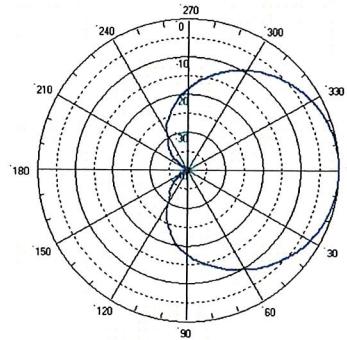
BROADBAND 1710-2170 MHz

1710 - 2170		
1710-1880	1850-1990	1920-2170
H66° V7.2°	H64° V6.6°	H63° V6.3°
Fixed Tilt 0°, 2°, 4°, 6°	Fixed Tilt 0°, 2°, 4°, 6°	Fixed Tilt 0°, 2°, 4°, 6°

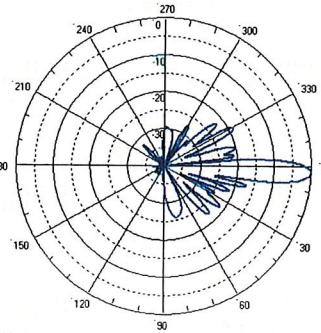


#### MECHANICAL SPECIFICATIONS

Connectors	2 X 7/16 Female
Connector Position	Bottom
Survival Wind Speed km/h (mph)	200 (125)
Front Windload N @ 160 km/h (lbs @ 100 mph)	370 (85)
Lateral Windload N @ 160 km/h (lbs @ 100 mph)	170 (40)
Radome Color	Grey, paintable
Humidity	100%
Antenna Weight kg (lbs)	7 (15)
Antenna Dimension mm (in) H X W X D	1340 X 170 X 100 (53 X 7 X 4)



H&V Pattern



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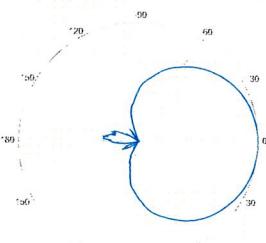
**BXA-70063-6CF-EDIN-X**

X-Pol | FET Panel | 63° | 14.5 dBd

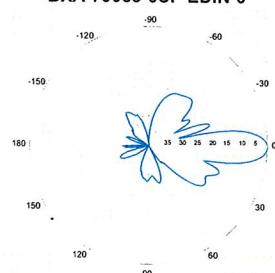
Replace "X" with desired electrical downtilt.

Antenna is also available with NE connector(s). Replace "EDIN" with "NE" in the model number when ordering.

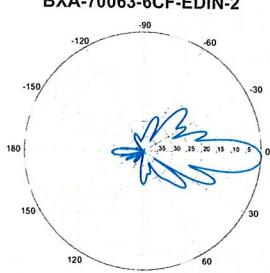
Electrical Characteristics		696-900 MHz	
Frequency bands		696-806 MHz	806-900 MHz
Polarization			±45°
Horizontal beamwidth		65°	63°
Vertical beamwidth		13°	11°
Gain		14.0 dBd (16.1 dBi)	14.5 dBd (16.6 dBi)
Electrical downtilt (X)		0, 2, 3, 4, 5, 6, 8, 10	
Impedance		50Ω	
VSWR		≤1.35:1	
Upper sidelobe suppression (0°)		-18.3 dB	-18.2 dB
Front-to-back ratio (+/-30°)		-33.4 dB	-36.3 dB
Null fill		5% (-26.02 dB)	< -25 dB
Isolation between ports			
Input power		500 W	
Lightning protection		Direct Ground	
Connector(s)		2 Ports / EDIN or NE / Female / Center (Back)	
Mechanical Characteristics			
Dimensions Length x Width x Depth		1804 x 285 x 132 mm	71.0 x 11.2 x 5.2 in
Depth with z-brackets		172 mm	6.8 in
Weight without mounting brackets		7.9 kg	17 lbs
Survival wind speed		> 201 km/hr	> 125 mph
Wind area	Front: 0.51 m <sup>2</sup>	Side: 0.24 m <sup>2</sup>	Front: 5.5 ft <sup>2</sup>
Wind load @ 161 km/hr (100 mph)	Front: 759 N	Side: 391 N	Side: 2.6 ft <sup>2</sup>
Front: 169 lbf	Front: 169 lbf	Side: 89 lbf	Side: 89 lbf
Mounting Options			
Part Number	Fits Pipe Diameter		Weight
36210003	50-160 mm	2.0-6.3 in	6.3 kg 14 lbs
36210004	50-160 mm	2.0-6.3 in	7.3 kg 16 lbs
A mounting bracket and downtilt bracket kit must be ordered for downtilt applications			
For concealment configurations, order BXA-70063-6CF-EDIN-X-FP			

**BXA-70063-6CF-EDIN-X**

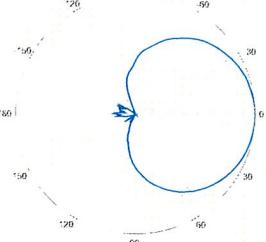
Horizontal | 750 MHz

**BXA-70063-6CF-EDIN-0**

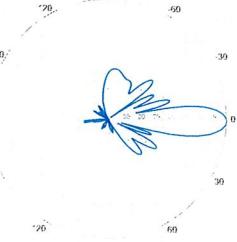
0° | Vertical | 750 MHz

**BXA-70063-6CF-EDIN-2**

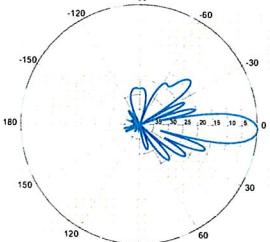
2° | Vertical | 750 MHz

**BXA-70063-6CF-EDIN-X**

Horizontal | 850 MHz



0° | Vertical | 850 MHz

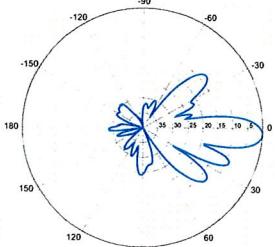


2° | Vertical | 850 MHz

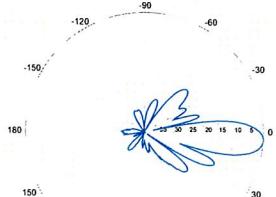
Quoted performance parameters are provided to offer typical or range values only and may vary as a result of normal manufacturing and operational conditions. Extreme operational conditions and/or stress on structural supports is beyond our control. Such conditions may result in damage to this product. Improvements to product may be made without notice.

**BXA-70063-6CF-EDIN-X**

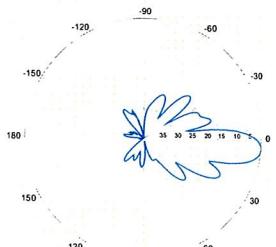
X-Pol | FET Panel | 63° | 14.5 dBd

**BXA-70063-6CF-EDIN-3**


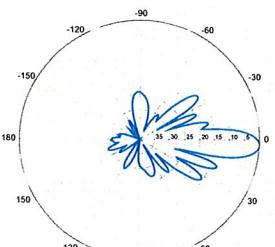
3° | Vertical | 750 MHz

**BXA-70063-6CF-EDIN-4**


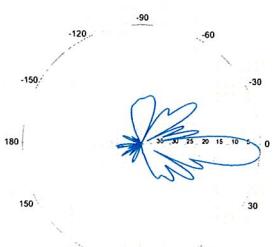
4° | Vertical | 750 MHz

**BXA-70063-6CF-EDIN-5**


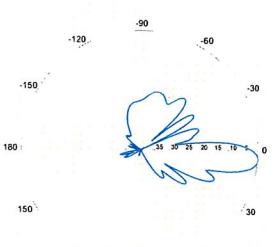
5° | Vertical | 750 MHz



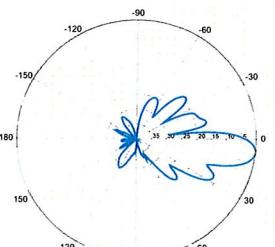
3° | Vertical | 850 MHz



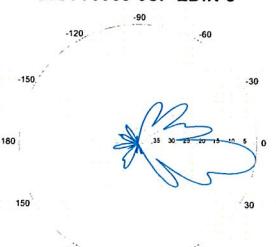
4° | Vertical | 850 MHz



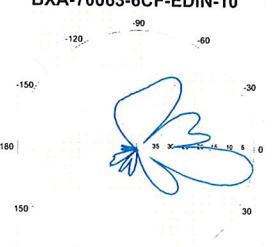
5° | Vertical | 850 MHz

**BXA-70063-6CF-EDIN-6**


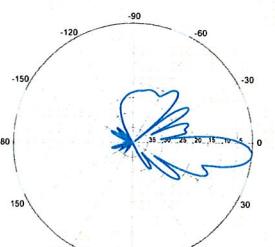
6° | Vertical | 750 MHz

**BXA-70063-6CF-EDIN-8**


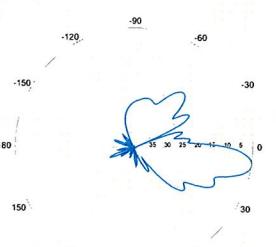
8° | Vertical | 750 MHz

**BXA-70063-6CF-EDIN-10**


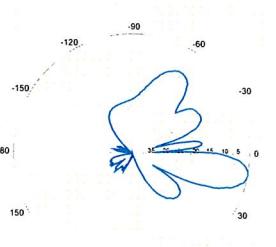
10° | Vertical | 750 MHz



6° | Vertical | 850 MHz



8° | Vertical | 850 MHz



10° | Vertical | 850 MHz

Quoted performance parameters are provided to offer typical or range values only and may vary as a result of normal manufacturing and operational conditions. Extreme operational conditions and/or stress on structural supports is beyond our control. Such conditions may result in damage to this product. Improvements to product may be made without notice.



## ShareLite Wideband Diplexer – In-line 698-960 MHz/1710-2200 MHz, DC pass in high frequency path

**Product Description**

The ShareLite FD9R6004 Series of diplexers are designed to enable feeder sharing between systems in the 698-960 MHz range and in the 1710-2200 MHz range. The diplexer is equipped with in-line connector placement so it can be installed in the BTS cabinet or at the tower top. This is especially valuable in crowded sites or when the feeders are not easily accessible. Due to its wideband design, the FD9R6004 Series can accommodate many combining solutions between 698-960 MHz and 1710-2200 MHz systems such as LTE 700 MHz, Cellular 800 MHz with PCS, GSM900 with GSM1800, or GSM900 with UMTS. This diplexer features a highly selective filter. It provides a high level of isolation between ports, while keeping the insertion loss on both paths at an extremely low level. The FD9R6004 diplexers are available with various DC pass options, helpful in configurations with or without the Tower Mount Amplifiers installed.

**Features/Benefits**

- LTE ready design
- Extremely Low Insertion Loss
- High level of Rejection between bands – Protection against interferences
- Extremely High Power Handling Capability
- Integrated DC block/bypass versions available
- Very compact & small size design – Easy installation and reduced tower load
- In-line long-neck connectors for easy connection & waterproofing
- Exceptional reliability & environmental protection (IP 67)
- Equipped with 1 \* Breathable Vent – Prevent any humidity inside the product
- Mounting hardware for Wall and Pole mount provided (P/N SEM2-1A)
- Grounding already provided through the mounting bracket
- Kit available for easy dual mount

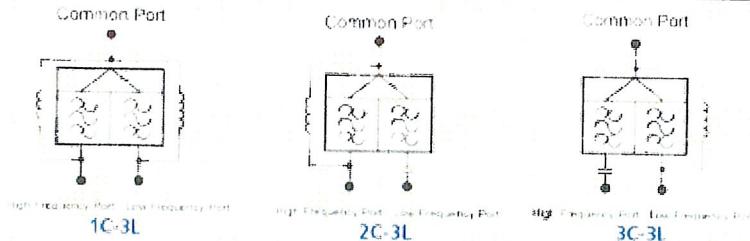
**Technical Specifications**

Product Type	Diplexer/Cross Band Coupler
Frequency Band, MHz	698-2200
Configuration	Sharelite Single diplexer, outdoor, DC pass in the 1710-2170MHz path, with mounting hardware SEM2-1A
Mounting	Wall Mounting: With 4 screws (maximum 6mm diameter); Pole Mounting: With included clamp set 40-110mm (1.57-4.33)
Frequency Range Low Frequency Path, MHz	698-960
Frequency Range High Frequency Path, MHz	1710-2200
Return Loss All Ports Min/Typ, dB	19/23
Power Handling Continuous, Max, W	1250 at common port; 750 in low frequency path & 500 in high frequency path
Power Handling Peak, Max, W	15000 in low frequency path & 8000 in high frequency path
Impedance, Ohms	50
Insertion Loss 698-960 MHz Path, Typ, dB	0.07
Insertion Loss 1710-2200MHz path, Typ, dB	0.13
Rejection Between Bands Min/Typ, dB	58/64@698-960MHz; 60/70@1710-2200MHz
IMP Level at the COM Port, Typ, dBm	-112 @ 2x43
DC Pass in Low Frequency Path	No
DC Pass in High Frequency Path	Yes
Temperature Range, °C (°F)	-40 to +60 (-40 to +140)
Environmental	ETSI 300-019-2-4 Class 4.1E
Ingress Protection	IP 67
Lightning Protection	EN/IEC61000-4-5 Level 4
Connectors	In-line long-neck 7-16-Female
Weight, kg (lb)	1.2 (2.6)
Shipping Weight, kg (lb)	3.2 (7) for 2 * single units in 1 * box, 9.8 (21.6) for 6 * units = 3 * Boxes in 1 * overwrap
Application	LTE 700MHz, GSM900/3G/UMTS, GSM900/GSM1800, Cellular 800/PCS
Dimensions, H x W x D, mm (in)	147 x 164 x 37 (5.8 x 6.5 x 1.5)
Shipping Dimensions, H x W x D, mm (in)	254 x 406 x 82 (10 x 16 x 3.2) for 2 * Single Units in 1 * box, 280 x 406 x 241 (11 x 16 x 9.5) for 6 * units = 3 * Boxes in 1 * overwrap
Volume, L	0.43
Housing	Aluminum

**Notes**

## ShareLite Wideband Diplexer – In-line 698-960 MHz/1710-2200 MHz, DC pass in high frequency path

Selection Guide Diplexer 698-960 / 1710-2200MHz					
	Model Number	Full DC Pass	DC Pass High Band	DC Pass Low Band	Mounting Hardware Included
Single	FD9R6004/1C-3L				X
	FD9R6004/2C-3L				X
	FD9R6004/3C-3L				X
Dual	KIT-FD9R6004/1C-DL				X
	KIT-FD9R6004/2C-DL				X
	KIT-FD9R6004/3C-DL				X



The FD9R6004 Series is upgradeable to a Dual Diplexer kit by means of 2 diplexers and mounting hardware kits SEM2-1A and SEM2-3.

## Mounting Hardware and Ground Cable Ordering Information

Model Number	Description	Image
SEM2-1A	Mounting Hardware, Pole mount ø40-110mm (Included with the Single and Dual Diplexer) Wall Screws M6 (Not included with the product)	
SEM2-3	Assembly kit for 2 pcs of FT9DW/xC-3L. (Can be ordered separately but included with the Dual Diplexer Kit)	
CA020-2	Ground Cable, 2m, includes lugs (Optional)	
CA030-2	Ground Cable, 2m, includes lugs (Optional)	
SEM6	Mounting Hardware for 6 Diplexers, Tower Base (Optional)	





Centered on Solutions™

## Structural Analysis Report

180' Existing ROHN Lattice Tower

Proposed Verizon Wireless  
LTE Antenna Installation

Verizon Site Ref: Wolcott North

1192 Wolcott Rd.  
Wolcott, CT

Centek Project No. 11001.CO1

Date: January 24, 2011



**Prepared for:**  
Verizon Wireless  
99 East River Road, 9<sup>th</sup> Floor  
East Hartford, CT 06108

**CENTEK** Engineering, Inc.

Structural Analysis - 180-ft ROHN Lattice Tower

Verizon Wireless LTE Antenna Installation

Wolcott, CT

January 24, 2011

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- VERIZON RF DATA SHEET.
- ANTENNA CUT SHEETS.

**CENTEK Engineering, Inc.**

*Structural Analysis - 180-ft ROHN Lattice Tower  
Verizon Wireless LTE Antenna Installation  
Wolcott, CT  
January 24, 2011*

## Introduction

The purpose of this report is to summarize the results of the non-linear, P-Δ structural analysis of the antenna installation proposed by Verizon Wireless on the existing self supporting lattice tower located in Wolcott, Connecticut.

The host tower is a 180-ft, three legged, tapered lattice tower originally designed and manufactured by ROHN, eng. file no. 23963DB dated November 28 1988. The tower geometry, structure member sizes and foundation information were taken from a previous structural analysis report prepared by URS Corp., job no. 36931099 (VZ4-023); dated November 5, 2007.

Antenna and appurtenance inventory were taken from the aforementioned URS structural report and a visual verification from grade by Centek Engineering personal on January 17, 2011.

The tower is made of nine (9) tapered vertical sections consisting of ROHN steel pipe legs. Diagonal and horizontal lateral support bracing consists of steel angle shapes. All connections were bolted connections. The width of the tower face is 6.52-ft at the top and 20.78-ft at the base.

Verizon Wireless proposes the removal of twelve (12) panel antennas and the installation of twelve (12) panel antennas and six (6) diplexers. Refer to the Antenna and Appurtenance Summary below for a detailed description of the proposed antenna configuration.

## Antenna and Appurtenance Summary

The existing tower supports several communication antennas. The existing and proposed loads considered in the analysis consist of the following:

- UNKNOWN (Existing):  
Antenna: One (1) 2-Bay Dipole and two (2) 10' Omni-Directional whips mounted on three (3) 3' stand-offs and one (1) 10' Omni-Directional whip flush mounted to a leg of the existing tower with a RAD center elevation of ±185-ft above grade level.  
Coax Cable: Three (3) 7/8" Ø and one (1) 1-1/4" Ø coax cables running on a leg/face of the existing tower as specified in Section 3 of this report.
- UNKNOWN (Existing):  
Antenna: One (1) 10' Omni-Directional whip mounted on one (1) 3' stand-off with a RAD center elevation of ±155-ft above grade level.  
Coax Cable: One (1) 7/8" Ø coax cable running on a leg/face of the existing tower as specified in Section 3 of this report.
- UNKNOWN (Existing):  
Antenna: Two (2) empty 3' stand-offs with an elevation of ±150-ft above grade level.
- UNKNOWN (Existing):  
Antenna: One (1) 8' Omni-Directional whip mounted on one (1) 2' stand-off with a RAD center elevation of ±144-ft above grade level.  
Coax Cable: One (1) 7/8" Ø coax cable running on a leg/face of the existing tower as specified in Section 3 of this report.

- **UNKNOWN (Existing):**  
Antenna: One (1) 8' Omni-Directional whip mounted on one (1) 2' stand-off with a RAD center elevation of ±104-ft above grade level.  
Coax Cable: One (1) 1/2" Ø coax cable running on a leg/face of the existing tower as specified in Section 3 of this report.
- **VERIZON (Existing to Remain):**  
Coax Cables: Twelve (12) 1-5/8" Ø coax cables running on a leg/face of the existing tower as specified in Section 3 of this report.
- **VERIZON (Existing to Remove):**  
Antennas: Six (6) Antel WPA-70063/6CF and six (6) Andrew 950F65T2ZE-M panel antennas mounted on three (3) PiROD 13' KD T-Frames with a RAD center elevation of ±135-ft above grade level.
- **VERIZON (Proposed):**  
Antennas: Three (3) Antel BXA-70063/6CF, four (4) RFS APL868013-42T0, two (2) RFS APL866513-42T0, two (2) RFS APX18-206516L-T0 and one (1) RYMSA MG D3-800T0 panel antennas and six (6) FD9R6004/2C-3L Diplexers mounted on three (3) existing PiROD 13' KD T-Frames with a RAD center elevation of ±135-ft above grade level.

### Primary Assumptions Used in the Analysis

- The tower structure's theoretical capacity not including any assessment of the condition of the tower.
- The tower carries the horizontal and vertical loads due to the weight of antennas, ice load and wind.
- Tower is properly installed and maintained.
- Tower is in plumb condition.
- Tower loading for antennas and mounts as listed in this report.
- All bolts are appropriately tightened providing the necessary connection continuity.
- All welds are fabricated with ER-70S-6 electrodes.
- All members are assumed to be as specified in the original tower design documents.
- All members are "hot dipped" galvanized in accordance with ASTM A123 and ASTM A153 Standards.
- All member protective coatings are in good condition.
- All tower members were properly designed, detailed, fabricated, installed and have been properly maintained since erection.
- Any deviation from the analyzed antenna loading will require a new analysis for verification of structural adequacy.
- **All coax cables routed as specified in Section 3 of this report.**

**CENTEK** Engineering, Inc.

Structural Analysis - 180-ft ROHN Lattice Tower  
Verizon Wireless LTE Antenna Installation  
Wolcott, CT  
January 24, 2011

## Analysis

The existing tower was analyzed using a comprehensive computer program entitled RISATower. The program analyzes the tower, considering the worst case loading condition. The tower is considered as loaded by concentric forces along the tower legs, and the model assumes that the leg members are subjected to bending, axial, and shear forces.

The existing tower was analyzed for 85 mph basic wind speed (fastest mile) with no ice and 75% reduction of wind force with  $\frac{1}{2}$  inch accumulative ice to determine stresses in members as per guidelines of TIA/EIA-222-F-96 entitled "Structural Standards for Steel Antenna Towers and Antenna Supporting Structures", the American Institute of Steel Construction (AISC) and the Manual of Steel Construction; Allowable Stress Design (ASD).

## Tower Loading

Tower loading was determined by the basic wind speed as applied to projected surface areas with modification factors per TIA/EIA-222-F, gravity loads of the tower structure and its components, and the application of  $\frac{1}{2}$ " radial ice tower structure and its components.

Basic Wind Speed:	New Haven; $v = 85$ mph (fastest mile)  Wolcott; $v = 95$ mph (3 second gust equivalent to $v = 77.5$ mph (fastest mile))  <i>TIA/EIA wind speed Controls</i>	[Section 16 of TIA/EIA-222-F-96]  [Appendix K of the 2005 CT Building Code Supplement]
Load Cases:	<u>Load Case 1</u> ; 85 mph wind speed w/ no ice plus gravity load – used in calculation of tower stresses and rotation. This load case typically controls the design.  <u>Load Case 2</u> ; 74 mph wind speed w/ $\frac{1}{2}$ " radial ice plus gravity load – used in calculation of tower stresses. The 74 mph wind speed velocity represents 75% of the wind pressure generated by the 85 mph wind speed.	[Section 2.3.16 of TIA/EIA-222-F-96]  [Section 2.3.16 of TIA/EIA-222-F-96]
	<u>Load Case 3</u> ; Seismic – not checked	[Section 1614.5 of State Bldg. Code 2005] does not control in the design of this structure type

## Tower Capacity

Tower stresses were calculated utilizing the structural analysis software RISATower. Allowable stresses were determined based on Table 5 of the TIA/EIA code with a 1/3 increase per Section 3.1.1.1 of the same code.

Calculated stresses were found to be within allowable limits. In Load Case 1, per RISATower "Section Capacity Table", this tower was found to be at **98.2%** of its total capacity.

Tower Section	Elevation	Stress Ratio (percentage of capacity)	Result
Diagonal (T10)	20'-0"-40'-0"	87.2%	PASS
Leg (T10)	20'-0"-40'-0"	98.2%	PASS

## Foundation and Anchors

The existing foundation consists of a 28.5-ft wide by 4.0-ft deep reinforced concrete mat footing. The sub grade conditions used in the analysis of the existing foundation were derived from the aforementioned URS structural report.

Tower legs are connected to the concrete mat by means of (4) 1.00"Ø, ASTM A354 Gr. BC anchor bolts per leg, embedded into the concrete mat.

Review of the foundation and anchor design consisted of verification of applied loads obtained from the tower design calculations and code checks of allowable stresses:

- The tower reactions developed from the governing Load Case 1 were used in the verification of the foundation:

Reactions	Vector	Proposed Load (kips, kip-ft)
Base	Shear	23
	Compression	16
	Moment	2170
Leg	Shear	14
	Compression	126
	Uplift	106

**CENTEK** Engineering, Inc.

Structural Analysis - 180-ft ROHN Lattice Tower  
Verizon Wireless LTE Antenna Installation  
Wolcott, CT  
January 24, 2011

- The anchor bolts were found to be within allowable limits.

Tower Section	Component	Stress Ratio (percentage of capacity)	Result
Anchor Bolts	Tension	50.3%	PASS

- The foundation was found to be within allowable limits.

Foundation	Design Limit	IBC 2003/2005 CT State Building Code Section 3108.4.2 (FS) <sup>(1)</sup>	Proposed Loading (FS) <sup>(1)</sup>	Result
Reinforced Concrete Mat	OM <sup>(2)</sup>	2.0	3.1	PASS

Note 1: FS denotes Factor of Safety

Note 2: OM denotes Overturning Moment

### Conclusion

This analysis shows that the subject tower is adequate to support the proposed antenna configuration.

The analysis is based, in part, on the information provided to this office by Verizon Wireless. If the existing conditions are different than the information in this report, Centek Engineering, Inc. must be contacted for resolution of any potential issues.

Please feel free to call with any questions or comments.

Respectfully Submitted by:

Checked by:

Carlo F. Centore, PE  
Principal ~ Structural Engineer



Prepared by:

Timothy J. Lynn, EIT  
Structural Engineer

**CENTEK** Engineering, Inc.

Structural Analysis - 180-ft ROHN Lattice Tower  
Verizon Wireless LTE Antenna Installation  
Wolcott, CT  
January 24, 2011

**Standard Conditions for Furnishing of Professional Engineering Services on Existing Structures**

All engineering services are performed on the basis that the information used is current and correct. This information may consist of, but is not necessarily limited to:

- Information supplied by the client regarding the structure itself, its foundations, the soil conditions, the antenna and feed line loading on the structure and its components, or other relevant information.
- Information from the field and/or drawings in the possession of Centek Engineering, Inc. or generated by field inspections or measurements of the structure.
- It is the responsibility of the client to ensure that the information provided to Centek Engineering, Inc. and used in the performance of our engineering services is correct and complete. In the absence of information to the contrary, we assume that all structures were constructed in accordance with the drawings and specifications and are in an un-corroded condition and have not deteriorated. It is therefore assumed that its capacity has not significantly changed from the "as new" condition.
- All services will be performed to the codes specified by the client, and we do not imply to meet any other codes or requirements unless explicitly agreed in writing. If wind and ice loads or other relevant parameters are to be different from the minimum values recommended by the codes, the client shall specify the exact requirement. In the absence of information to the contrary, all work will be performed in accordance with the latest revision of ANSI/ASCE10 & ANSI/EIA-222
- All services performed, results obtained, and recommendations made are in accordance with generally accepted engineering principles and practices. Centek Engineering, Inc. is not responsible for the conclusions, opinions and recommendations made by others based on the information we supply.

**CENTEK** Engineering, Inc.

*Structural Analysis - 180-ft RÖHN Lattice Tower*

*Verizon Wireless LTE Antenna Installation*

*Wolcott, CT*

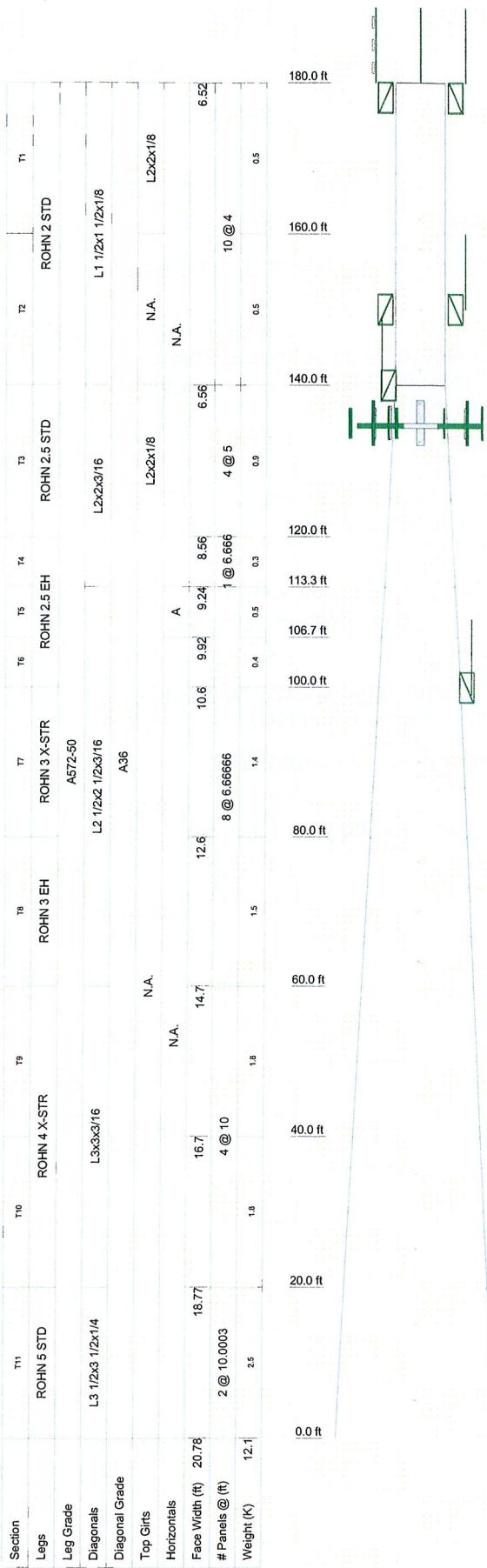
*January 24, 2011*

## GENERAL DESCRIPTION OF STRUCTURAL ANALYSIS PROGRAM

RISATower, is an integrated structural analysis and design software package for Designed specifically for the telecommunications industry, RISATower, formerly ERITower, automates much of the tower analysis and design required by the TIA/EIA 222 Standard.

### RISATower Features:

- RISATower can analyze and design 3- and 4-sided guyed towers, 3- and 4-sided self-supporting towers and either round or tapered ground mounted poles with or without guys.
- The program analyzes towers using the TIA-222-G (2005) standard or any of the previous TIA/EIA standards back to RS-222 (1959). Steel design is checked using the AISC ASD 9th Edition or the AISC LRFD specifications.
- Linear and non-linear (P-delta) analyses can be used in determining displacements and forces in the structure. Wind pressures and forces are automatically calculated.
- Extensive graphics plots include material take-off, shear-moment, leg compression, displacement, twist, feed line, guy anchor and stress plots.
- RISATower contains unique features such as True Cable behavior, hog rod take-up, foundation stiffness and much more.



### DESIGNED APPURTENANCE LOADING

TYPE	ELEVATION	TYPE	ELEVATION
2 Bay Dipole	185	BXA-70063/6CF (Verizon - Proposed)	135
2" Dia 10' Omni	185	APX18-206516L-T0 (Verizon - Proposed)	135
2" Dia 10' Omni	185	APL868013-42T0 (Verizon - Proposed)	135
2" Dia 10' Omni	185	APL868013-42T0 (Verizon - Proposed)	135
3' Side Mount Standoff	178	BXA-70063/6CF (Verizon - Proposed)	135
3' Side Mount Standoff	178	APX18-206516L-T0 (Verizon - Proposed)	135
3' Side Mount Standoff	178	APL868013-42T0 (Verizon - Proposed)	135
2" Dia 10' Omni	155	APL868013-42T0 (Verizon - Proposed)	135
3' Side Mount Standoff	150	APL868013-42T0 (Verizon - Proposed)	135
3' Side Mount Standoff	150	APL868013-42T0 (Verizon - Proposed)	135
2" Dia 8' Omni	144	Pirod 13 KD T-Frame	135
2' Side Mount Standoff	140	Pirod 13 KD T-Frame	135
BXA-70063/6CF (Verizon - Proposed)	135	Pirod 13 KD T-Frame	135
MG D3-800T0 (Verizon - Proposed)	135	2" Dia 8' Omni	104
APL868013-42T0 (Verizon - Proposed)	135	2' Side Mount Standoff	100

### SYMBOL LIST

MARK	SIZE	MARK	SIZE
A	L3x3x3/16		

### MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-50	50 ksi	65 ksi	A36	36 ksi	58 ksi

### TOWER DESIGN NOTES

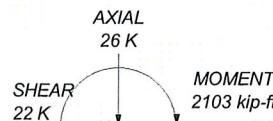
1. Tower is located in New Haven County, Connecticut.
2. Tower designed for a 85 mph basic wind in accordance with the TIA/EIA-222-F Standard.
3. Tower is also designed for a 74 mph basic wind with 0.50 in ice.
4. Deflections are based upon a 50 mph wind.
5. TOWER RATING: 98.2%

### MAX. CORNER REACTIONS AT BASE:

DOWN: 126 K

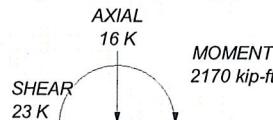
UPLIFT: -106 K

SHEAR: 14 K



TORQUE 15 kip-ft

74 mph WIND - 0.5000 in ICE



TORQUE 17 kip-ft

REACTIONS - 85 mph WIND

**Centeck Engineering Inc.**

63-2 North Branford Road

Branford, CT 06405

Phone: 203.488.0580

FAX: 203.488.8587

Job: 11001.CO4 ~ Wolcott North

Project: 180' Self-Support Lattice 1192 Wolcott Road., Wolcott, CT

Client: Verizon Wireless Drawn by: TJL App'd:

Code: TIA/EIA-222-F Date: 01/24/11 Scale: NTS

Path: J:\011001\01\1192\Wolcott\Wolcott\Wolcott.Lst Date: 01/24/11

Dwg No. E-1

## Feedline Plan

Round \_\_\_\_\_

Flat \_\_\_\_\_

App In Face

App Out Face

(6) verizon relocated 1 5/8      (6) verizon existing 1 5/8

7 1/8  
7 1/8  
(3) 1 1/4  
1/2

**Centek Engineering Inc.**  
63-2 North Branford Road  
Branford, CT 06405  
Phone: 203.488.0580  
FAX: 203.488.8587

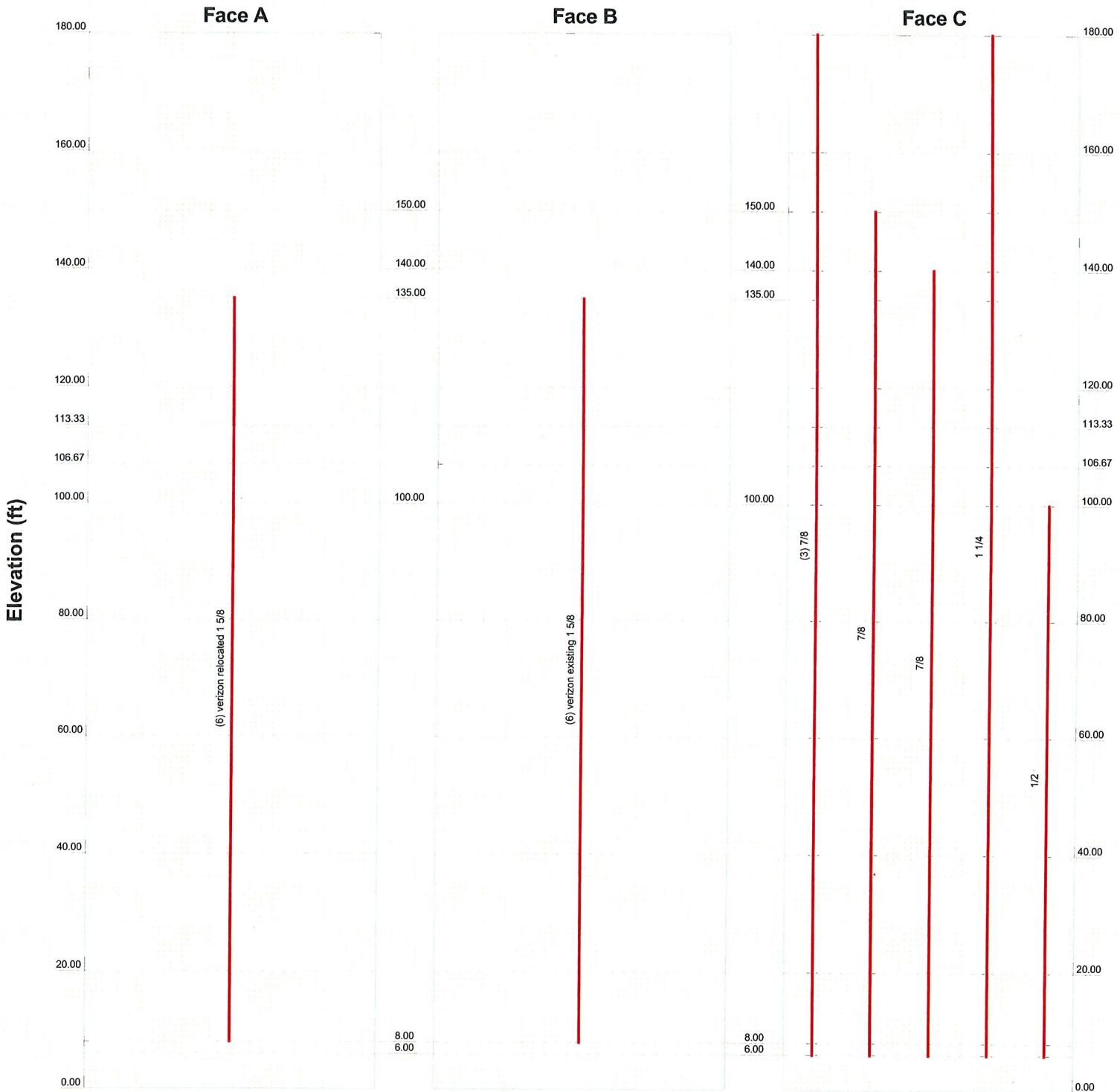
Job: **11001.CO4 ~ Wolcott North**

Client: Verizon Wireless	Drawn by: TJL	App'd:
Code: TIA/EIA-222-F	Date: 01/24/11	Scale: NTS
Path: J:\Net\11001\CO4\Wolcott North - 1192 Wolcott Road, Branford, CT\Gens\RI Files\180' ROLL RGHN Lattice Tower.dwg	Dwg No. E-7	

# Feedline Distribution Chart

0' - 180'

— Round    
 — Flat    
 — App In Face    
 — App Out Face    
 — Truss Leg



**Centek Engineering Inc.**  
 63-2 North Branford Road  
 Branford, CT 06405  
 Phone: 203.488.0580  
 FAX: 203.488.8587

Job: 11001.CO4 ~ Wolcott North	
Project: 180' Self-Support Lattice 1192 Wolcott Road, Wolcott, CT	
Client: Verizon Wireless	Drawn by: TJL
Code: TIA/EIA-222-F	Date: 01/24/11
Path: J:\Jobs\11001\02\WFCO1-Wolcott North - 1192 Wolcott Road, Wolcott, CT\Case\ER\Flat\180' ROHIN Lattice Tower.dwg	Scale: NTS
	Dwg No. E-7

<b>RISATower</b>  <b>Centek Engineering Inc.</b> <i>63-2 North Branford Road</i> <i>Branford, CT 06405</i> <i>Phone: 203.488.0580</i> <i>FAX: 203.488.8587</i>	<b>Job</b> 11001.CO4 ~ Wolcott North	<b>Page</b> 1 of 31
	<b>Project</b> 180' Self-Support Lattice 1192 Wolcott Road., Wolcott, CT	<b>Date</b> 16:40:36 01/24/11
	<b>Client</b> Verizon Wireless	<b>Designed by</b> TJL

## Tower Input Data

The main tower is a 3x free standing tower with an overall height of 180.00 ft above the ground line.

The base of the tower is set at an elevation of 0.00 ft above the ground line.

The face width of the tower is 6.52 ft at the top and 20.78 ft at the base.

This tower is designed using the TIA/EIA-222-F standard.

The following design criteria apply:

- Tower is located in New Haven County, Connecticut.
- Basic wind speed of 85 mph.
- Nominal ice thickness of 0.5000 in.
- Ice density of 56 pcf.
- A wind speed of 74 mph is used in combination with ice.
- Temperature drop of 50 °F.
- Deflections calculated using a wind speed of 50 mph.
- A non-linear (P-delta) analysis was used.
- Pressures are calculated at each section.
- Stress ratio used in tower member design is 1.333.
- Local bending stresses due to climbing loads, feedline supports, and appurtenance mounts are not considered.

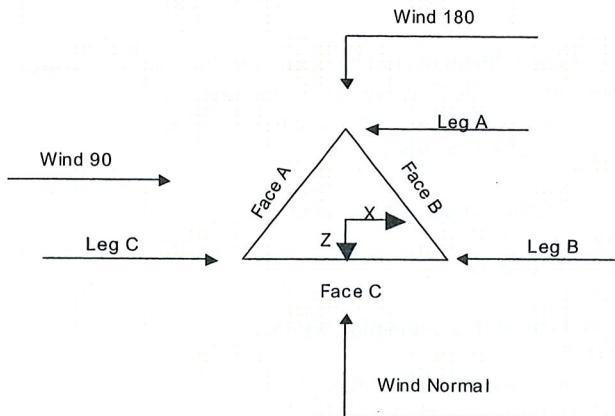
## Options

Consider Moments - Legs	Distribute Leg Loads As Uniform	Treat Feedline Bundles As Cylinder
Consider Moments - Horizontals	Assume Legs Pinned	Use ASCE 10 X-Brace Ly Rules
Consider Moments - Diagonals	✓ Assume Rigid Index Plate	Calculate Redundant Bracing Forces
Use Moment Magnification	✓ Use Clear Spans For Wind Area	Ignore Redundant Members in FEA
✓ Use Code Stress Ratios	✓ Use Clear Spans For KL/r	SR Leg Bolts Resist Compression
Use Code Safety Factors - Guys	Retension Guys To Initial Tension	✓ All Leg Panels Have Same Allowable
Escalate Ice	Bypass Mast Stability Checks	Offset Girt At Foundation
Always Use Max Kz	Use Azimuth Dish Coefficients	✓ Consider Feedline Torque
Use Special Wind Profile	✓ Project Wind Area of Appurt.	Include Angle Block Shear Check
✓ Include Bolts In Member Capacity	Autocalc Torque Arm Areas	Poles
✓ Leg Bolts Are At Top Of Section	SR Members Have Cut Ends	Include Shear-Torsion Interaction
Secondary Horizontal Braces Leg	✓ Sort Capacity Reports By Component	Always Use Sub-Critical Flow
Use Diamond Inner Bracing (4 Sided)	Triangulate Diamond Inner Bracing	Use Top Mounted Sockets
Add IBC .6D+W Combination		

# RISATower

**Centek Engineering Inc.**  
 63-2 North Branford Road  
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 FAX: 203.488.8587

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Client	Verizon Wireless	Designed by	TJL



**Triangular Tower**

## Tower Section Geometry

Tower Section	Tower Elevation	Assembly Database	Description	Section Width	Number of Sections	Section Length
				ft		ft
T1	180.00-160.00			6.52	1	20.00
T2	160.00-140.00			6.52	1	20.00
T3	140.00-120.00			6.56	1	20.00
T4	120.00-113.33			8.56	1	6.67
T5	113.33-106.67			9.24	1	6.67
T6	106.67-100.00			9.92	1	6.67
T7	100.00-80.00			10.60	1	20.00
T8	80.00-60.00			12.60	1	20.00
T9	60.00-40.00			14.70	1	20.00
T10	40.00-20.00			16.70	1	20.00
T11	20.00-0.00			18.77	1	20.00

## Tower Section Geometry (cont'd)

Tower Section	Tower Elevation	Diagonal Spacing	Bracing Type	Has K Brace End Panels	Has Horizontals	Top Girt Offset	Bottom Girt Offset
		ft	ft			in	in
T1	180.00-160.00	4.00	X Brace	No	No	0.0000	0.0000
T2	160.00-140.00	4.00	X Brace	No	No	0.0000	0.0000
T3	140.00-120.00	5.00	X Brace	No	No	0.0000	0.0000
T4	120.00-113.33	6.67	X Brace	No	No	0.0000	0.0000

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Tower Section	Tower Elevation	Diagonal Spacing	Bracing Type	Has K Brace End Panels	Has Horizontals	Top Girt Offset	Bottom Girt Offset
	ft	ft				in	in
T5	113.33-106.67	6.67	X Brace	No	Yes	0.0000	0.0000
T6	106.67-100.00	6.67	X Brace	No	No	0.0000	0.0000
T7	100.00-80.00	6.67	X Brace	No	No	0.0000	0.0000
T8	80.00-60.00	6.67	X Brace	No	No	0.0000	0.0000
T9	60.00-40.00	10.00	X Brace	No	No	0.0000	0.0000
T10	40.00-20.00	10.00	X Brace	No	No	0.0000	0.0000
T11	20.00-0.00	10.00	X Brace	No	No	0.0000	0.0000

## Tower Section Geometry (cont'd)

Tower Elevation ft	Leg Type	Leg Size	Leg Grade	Diagonal Type	Diagonal Size	Diagonal Grade
T1 180.00-160.00	Pipe	ROHN 2 STD	A572-50 (50 ksi)	Single Angle	L1 1/2x1 1/2x1/8	A36 (36 ksi)
T2 160.00-140.00	Pipe	ROHN 2 STD	A572-50 (50 ksi)	Single Angle	L1 1/2x1 1/2x1/8	A36 (36 ksi)
T3 140.00-120.00	Pipe	ROHN 2.5 STD	A572-50 (50 ksi)	Single Angle	L2x2x3/16	A36 (36 ksi)
T4 120.00-113.33	Pipe	ROHN 2.5 EH	A572-50 (50 ksi)	Single Angle	L2x2x3/16	A36 (36 ksi)
T5 113.33-106.67	Pipe	ROHN 2.5 EH	A572-50 (50 ksi)	Single Angle	L2 1/2x2 1/2x3/16	A36 (36 ksi)
T6 106.67-100.00	Pipe	ROHN 2.5 EH	A572-50 (50 ksi)	Single Angle	L2 1/2x2 1/2x3/16	A36 (36 ksi)
T7 100.00-80.00	Pipe	ROHN 3 X-STR	A572-50 (50 ksi)	Single Angle	L2 1/2x2 1/2x3/16	A36 (36 ksi)
T8 80.00-60.00	Pipe	ROHN 3 EH	A572-50 (50 ksi)	Single Angle	L2 1/2x2 1/2x3/16	A36 (36 ksi)
T9 60.00-40.00	Pipe	ROHN 4 X-STR	A572-50 (50 ksi)	Single Angle	L3x3x3/16	A36 (36 ksi)
T10 40.00-20.00	Pipe	ROHN 4 X-STR	A572-50 (50 ksi)	Single Angle	L3x3x3/16	A36 (36 ksi)
T11 20.00-0.00	Pipe	ROHN 5 STD	A572-50 (50 ksi)	Single Angle	L3 1/2x3 1/2x1/4	A36 (36 ksi)

## Tower Section Geometry (cont'd)

Tower Elevation ft	Top Girt Type	Top Girt Size	Top Girt Grade	Bottom Girt Type	Bottom Girt Size	Bottom Girt Grade
T1 180.00-160.00	Equal Angle	L2x2x1/8	A36 (36 ksi)	Solid Round		A572-50 (50 ksi)
T3 140.00-120.00	Single Angle	L2x2x1/8	A36 (36 ksi)	Solid Round		A572-50 (50 ksi)

## Tower Section Geometry (cont'd)

<b>RISATower</b>  <b>Centek Engineering Inc.</b> <i>63-2 North Branford Road</i> <i>Branford, CT 06405</i> <i>Phone: 203.488.0580</i> <i>FAX: 203.488.8587</i>	<b>Job</b>	11001.CO4 ~ Wolcott North	<b>Page</b>
	<b>Project</b>	180' Self-Support Lattice 1192 Wolcott Road., Wolcott, CT	<b>Date</b> 16:40:36 01/24/11
	<b>Client</b>	Verizon Wireless	<b>Designed by</b> TJL

Tower Elevation ft	No. of Mid Girts	Mid Girt Type	Mid Girt Size	Mid Girt Grade	Horizontal Type	Horizontal Size	Horizontal Grade
T5 113.33-106.67	None	Single Angle		A36 (36 ksi)	Single Angle	L3x3x3/16	A36 (36 ksi)

## Tower Section Geometry (cont'd)

Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade	Adjust. Factor $A_f$	Adjust. Factor $A_r$	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals	Double Angle Stitch Bolt Spacing Horizontals
ft	ft <sup>2</sup>	in					in	in
T1 180.00-160.00	0.00	0.0000	A36 (36 ksi)	1.02	1	1.02	36.0000	36.0000
T2 160.00-140.00	0.00	0.0000	A36 (36 ksi)	1.02	1	1.02	36.0000	36.0000
T3 140.00-120.00	0.00	0.0000	A36 (36 ksi)	1.02	1	1.02	36.0000	36.0000
T4 120.00-113.33	0.00	0.0000	A36 (36 ksi)	1.02	1	1.02	36.0000	36.0000
T5 113.33-106.67	0.00	0.0000	A36 (36 ksi)	1.02	1	1.02	36.0000	36.0000
T6 106.67-100.00	0.00	0.0000	A36 (36 ksi)	1.02	1	1.02	36.0000	36.0000
T7 100.00-80.00	0.00	0.0000	A36 (36 ksi)	1.02	1	1.02	36.0000	36.0000
T8 80.00-60.00	0.00	0.0000	A36 (36 ksi)	1.02	1	1.02	36.0000	36.0000
T9 60.00-40.00	0.00	0.0000	A36 (36 ksi)	1.02	1	1.02	36.0000	36.0000
T10 40.00-20.00	0.00	0.0000	A36 (36 ksi)	1.02	1	1.02	36.0000	36.0000
T11 20.00-0.00	0.00	0.0000	A36 (36 ksi)	1.02	1	1.02	36.0000	36.0000

## Tower Section Geometry (cont'd)

# RISATower

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Tower Elevation ft	Calc K Single Angles	Calc K Solid Rounds	Legs	K Factors <sup>1</sup>							
				X Brace Diags		K Brace Diags		Single Diags		Girts	
				X	Y	X	Y	X	Y	X	Y
T6 106.67- 100.00	Yes	Yes	1	1	1	1	1	1	1	1	1
T7 100.00- 80.00	Yes	Yes	1	1	1	1	1	1	1	1	1
T8 80.00- 60.00	Yes	Yes	1	1	1	1	1	1	1	1	1
T9 60.00- 40.00	Yes	Yes	1	1	1	1	1	1	1	1	1
T10 40.00- 20.00	Yes	Yes	1	1	1	1	1	1	1	1	1
T11 20.00- 0.00	Yes	Yes	1	1	1	1	1	1	1	1	1

<sup>1</sup>Note: K factors are applied to member segment lengths. K-braces without inner supporting members will have the K factor in the out-of-plane direction applied to the overall length.

## Tower Section Geometry (cont'd)

Tower Elevation ft	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal	Short Horizontal
	Net Width Deduct in	U										
T1 180.00- 160.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T2 160.00- 140.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T3 140.00- 120.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T4 120.00- 113.33	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T5 113.33- 106.67	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T6 106.67- 100.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T7 100.00- 80.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T8 80.00-60.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T9 60.00-40.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T10 40.00- 20.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1
T11 20.00-0.00	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1	0.0000	1

## Tower Section Geometry (cont'd)

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	Client	Designed by
	Verizon Wireless	TJL

Tower Elevation ft	Leg Connection Type	Leg	Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal		
			Bolt Size in	No.	Bolt Size in	No.	Bolt Size in	No.							
T1 180.00-160.00	Flange	0.6250	0	0.6250	1	0.6250	0	0.6250	0	0.6250	0	0.5000	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T2 160.00-140.00	Flange	0.6250	4	0.6250	1	0.6250	0	0.6250	0	0.6250	0	0.5000	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T3 140.00-120.00	Flange	0.6250	4	0.6250	1	0.6250	0	0.6250	0	0.6250	0	0.5000	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T4 120.00-113.33	Flange	0.6250	4	0.6250	1	1.0000	0	0.6250	0	0.6250	0	0.5000	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T5 113.33-106.67	Flange	0.7500	0	0.6250	1	1.0000	0	0.6250	0	0.6250	0	0.5000	1	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T6 106.67-100.00	Flange	0.7500	0	0.6250	1	1.0000	0	0.6250	0	0.6250	0	0.5000	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T7 100.00-80.00	Flange	0.7500	4	0.6250	1	1.0000	0	0.6250	0	0.6250	0	0.5000	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T8 80.00-60.00	Flange	0.8750	4	0.6250	1	1.2500	0	0.6250	0	0.6250	0	0.5000	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325X		A325X	
T9 60.00-40.00	Flange	0.8750	4	0.6250	1	1.2500	0	0.6250	0	0.6250	0	0.5000	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325X		A325X	
T10 40.00-20.00	Flange	0.8750	4	0.6250	1	1.2500	0	0.6250	0	0.6250	0	0.5000	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325X		A325X	
T11 20.00-0.00	Flange	1.0000	4	0.6250	1	1.2500	0	0.6250	0	0.6250	0	0.5000	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325X		A325X	

## Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	# Per Row	#	Clear Spacing in	Width or Diameter in	Perimeter in	Weight plf
7/8	C	Yes	Ar (CfAe)	180.00 - 6.00	2.5000	0.41	3	3	1.1100 1.0000	1.1100	1.1100	0.54
7/8	C	Yes	Ar (CfAe)	150.00 - 6.00	2.5000	0.43	1	1	1.1100	1.1100	1.1100	0.54
7/8	C	Yes	Ar (CfAe)	140.00 - 6.00	2.5000	0.44	1	1	1.1100 1.0000	1.1100	1.1100	0.54
1 1/4	C	Yes	Ar (CfAe)	180.00 - 6.00	2.5000	0.39	1	1	1.5500	1.5500	1.5500	0.66
1/2	C	Yes	Ar (CfAe)	100.00 - 6.00	2.5000	0.35	1	1	0.5800	0.5800	0.5800	0.58
verizon existing 1 5/8 verizon relocated 1 5/8	B	Yes	Ar (CfAe)	135.00 - 8.00	2.5000	-0.38	6	6	1.9800	1.9800	1.9800	1.04
	A	Yes	Ar (CfAe)	135.00 - 8.00	2.5000	0.38	6	6	1.9800	1.9800	1.9800	1.04

## Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation ft	Face	$A_R$ $ft^2$	$A_F$ $ft^2$	$C_A A_A$ In Face $ft^2$	$C_A A_A$ Out Face $ft^2$	Weight K
T1	180.00-160.00	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	8.133	0.000	0.000	0.000	0.05
T2	160.00-140.00	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00

# RISA Tower

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Project	180' Self-Support Lattice 1192 Wolcott Road., Wolcott, CT	7 of 31
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Tower Section	Tower Elevation ft	Face	$A_R$ ft <sup>2</sup>	$A_F$ ft <sup>2</sup>	$C_A A_A$ In Face ft <sup>2</sup>	$C_A A_A$ Out Face ft <sup>2</sup>	Weight
T3	140.00-120.00	C	9.058	0.000	0.000	0.000	0.05
		A	14.850	0.000	0.000	0.000	0.09
		B	14.850	0.000	0.000	0.000	0.09
T4	120.00-113.33	C	11.833	0.000	0.000	0.000	0.07
		A	6.599	0.000	0.000	0.000	0.04
		B	6.599	0.000	0.000	0.000	0.04
T5	113.33-106.67	C	3.944	0.000	0.000	0.000	0.02
		A	6.600	0.000	0.000	0.000	0.04
		B	6.600	0.000	0.000	0.000	0.04
T6	106.67-100.00	C	3.944	0.000	0.000	0.000	0.02
		A	6.600	0.000	0.000	0.000	0.04
		B	6.600	0.000	0.000	0.000	0.04
T7	100.00-80.00	C	19.800	0.000	0.000	0.000	0.02
		A	19.800	0.000	0.000	0.000	0.12
		B	19.800	0.000	0.000	0.000	0.12
T8	80.00-60.00	C	12.800	0.000	0.000	0.000	0.08
		A	19.800	0.000	0.000	0.000	0.12
		B	19.800	0.000	0.000	0.000	0.12
T9	60.00-40.00	C	12.800	0.000	0.000	0.000	0.08
		A	19.800	0.000	0.000	0.000	0.12
		B	19.800	0.000	0.000	0.000	0.12
T10	40.00-20.00	C	12.800	0.000	0.000	0.000	0.08
		A	19.800	0.000	0.000	0.000	0.12
		B	19.800	0.000	0.000	0.000	0.12
T11	20.00-0.00	C	12.800	0.000	0.000	0.000	0.08
		A	11.881	0.000	0.000	0.000	0.07
		B	11.881	0.000	0.000	0.000	0.07
		C	8.960	0.000	0.000	0.000	0.06

## Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	$A_R$ ft <sup>2</sup>	$A_F$ ft <sup>2</sup>	$C_A A_A$ In Face ft <sup>2</sup>	$C_A A_A$ Out Face ft <sup>2</sup>	Weight
T1	180.00-160.00	A	0.500	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		14.800	0.000	0.000	0.000	0.13
T2	160.00-140.00	A	0.500	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		16.558	0.000	0.000	0.000	0.14
T3	140.00-120.00	A	0.500	22.350	0.000	0.000	0.000	0.23
		B		22.350	0.000	0.000	0.000	0.23
		C		21.833	0.000	0.000	0.000	0.19
T4	120.00-113.33	A	0.500	9.932	0.000	0.000	0.000	0.10
		B		9.932	0.000	0.000	0.000	0.10
		C		7.277	0.000	0.000	0.000	0.06
T5	113.33-106.67	A	0.500	9.933	0.000	0.000	0.000	0.10
		B		9.933	0.000	0.000	0.000	0.10
		C		7.278	0.000	0.000	0.000	0.06
T6	106.67-100.00	A	0.500	9.933	0.000	0.000	0.000	0.10
		B		9.933	0.000	0.000	0.000	0.10
		C		7.278	0.000	0.000	0.000	0.06
T7	100.00-80.00	A	0.500	29.800	0.000	0.000	0.000	0.31
		B		29.800	0.000	0.000	0.000	0.31
		C		24.467	0.000	0.000	0.000	0.22
T8	80.00-60.00	A	0.500	29.800	0.000	0.000	0.000	0.31
		B		29.800	0.000	0.000	0.000	0.31
		C		24.467	0.000	0.000	0.000	0.22

# RISA Tower

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	Client	Verizon Wireless	Designed by TJL

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	$A_R$ ft <sup>2</sup>	$A_F$ ft <sup>2</sup>	$C_{AA}$ In Face ft <sup>2</sup>	$C_{AA}$ Out Face ft <sup>2</sup>	Weight K
T9	60.00-40.00	A	0.500	29.800	0.000	0.000	0.000	0.31
		B		29.800	0.000	0.000	0.000	0.31
		C		24.467	0.000	0.000	0.000	0.22
T10	40.00-20.00	A	0.500	29.800	0.000	0.000	0.000	0.31
		B		29.800	0.000	0.000	0.000	0.31
		C		24.467	0.000	0.000	0.000	0.22
T11	20.00-0.00	A	0.500	17.881	0.000	0.000	0.000	0.18
		B		17.881	0.000	0.000	0.000	0.18
		C		17.127	0.000	0.000	0.000	0.15

## Feed Line Shielding

Section	Elevation	Face	$A_R$	$A_R$ Ice	$A_F$	$A_F$ Ice
	ft		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>
T1	180.00-160.00	A	0.000	0.000	0.000	0.000
		B	0.000	0.000	0.000	0.000
		C	0.000	0.785	0.664	1.209
T2	160.00-140.00	A	0.000	0.000	0.000	0.000
		B	0.000	0.000	0.000	0.000
		C	0.000	0.809	0.664	1.213
T3	140.00-120.00	A	0.000	0.988	1.313	1.977
		B	0.000	0.988	1.313	1.977
		C	0.000	0.965	1.047	1.931
T4	120.00-113.33	A	0.000	0.310	0.412	0.620
		B	0.000	0.310	0.412	0.620
		C	0.000	0.227	0.246	0.455
T5	113.33-106.67	A	0.000	0.427	0.750	1.129
		B	0.000	0.427	0.750	1.129
		C	0.000	0.313	0.448	0.827
T6	106.67-100.00	A	0.000	0.296	0.492	0.740
		B	0.000	0.296	0.492	0.740
		C	0.000	0.217	0.294	0.542
T7	100.00-80.00	A	0.000	0.860	1.428	2.150
		B	0.000	0.860	1.428	2.150
		C	0.000	0.706	0.923	1.765
T8	80.00-60.00	A	0.000	0.829	1.378	2.074
		B	0.000	0.829	1.378	2.074
		C	0.000	0.681	0.891	1.703
T9	60.00-40.00	A	0.000	0.589	1.174	1.767
		B	0.000	0.589	1.174	1.767
		C	0.000	0.484	0.759	1.451
T10	40.00-20.00	A	0.000	0.570	1.137	1.711
		B	0.000	0.570	1.137	1.711
		C	0.000	0.468	0.735	1.405
T11	20.00-0.00	A	0.000	0.334	0.777	1.169
		B	0.000	0.334	0.777	1.169
		C	0.000	0.320	0.586	1.120

## Feed Line Center of Pressure

<p><b>RISATower</b></p> <p><b>Centek Engineering Inc.</b> 63-2 North Branford Road Branford, CT 06405 Phone: 203.488.0580 FAX: 203.488.8587</p>	Job	11001.CO4 ~ Wolcott North	Page
	Project	180' Self-Support Lattice 1192 Wolcott Road., Wolcott, CT	Date
	Client	Verizon Wireless	Designed by TJL

Section	Elevation	CP <sub>X</sub>	CP <sub>Z</sub>	CP <sub>X</sub> Ice in	CP <sub>Z</sub> Ice in
	ft	in	in		
T1	180.00-160.00	-3.7554	3.0573	-4.1217	3.3496
T2	160.00-140.00	-4.4197	3.5719	-4.8724	3.9305
T3	140.00-120.00	-3.8255	-8.8172	-4.5965	-7.9673
T4	120.00-113.33	-4.4478	-14.2139	-5.4036	-13.2986
T5	113.33-106.67	-3.5975	-11.4806	-4.4844	-11.0243
T6	106.67-100.00	-4.5651	-14.5513	-5.6851	-13.9630
T7	100.00-80.00	-5.0561	-14.7561	-6.5566	-14.0565
T8	80.00-60.00	-5.6661	-16.5015	-7.3605	-15.7567
T9	60.00-40.00	-6.1780	-17.9645	-8.3762	-17.9116
T10	40.00-20.00	-6.7494	-19.6026	-9.1653	-19.5828
T11	20.00-0.00	-4.8865	-11.5618	-7.0024	-11.9879

### Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C <sub>AA</sub> Front	C <sub>AA</sub> Side	Weight K	
APL868013-42T0 (Verizon - Proposed)	A	From Leg	3.00 6.00 0.00	0.0000	135.00	No Ice 1/2" Ice	2.87 3.18	3.73 4.10	0.02 0.04
BXA-70063/6CF (Verizon - Proposed)	A	From Leg	3.00 0.00 0.00	0.0000	135.00	No Ice 1/2" Ice	7.73 8.27	3.76 4.19	0.02 0.06
APX18-206516L-T0 (Verizon - Proposed)	A	From Leg	3.00 -4.00 0.00	0.0000	135.00	No Ice 1/2" Ice	3.51 3.85	2.00 2.33	0.02 0.04
APL868013-42T0 (Verizon - Proposed)	A	From Leg	3.00 -6.00 0.00	0.0000	135.00	No Ice 1/2" Ice	2.87 3.18	3.73 4.10	0.02 0.04
APL868013-42T0 (Verizon - Proposed)	B	From Leg	3.00 6.00 0.00	0.0000	135.00	No Ice 1/2" Ice	2.87 3.18	3.73 4.10	0.02 0.04
BXA-70063/6CF (Verizon - Proposed)	B	From Leg	3.00 0.00 0.00	0.0000	135.00	No Ice 1/2" Ice	7.73 8.27	3.76 4.19	0.02 0.06
MG D3-800T0 (Verizon - Proposed)	B	From Leg	3.00 -4.00 0.00	0.0000	135.00	No Ice 1/2" Ice	3.45 3.80	2.22 2.55	0.02 0.04
APL868013-42T0 (Verizon - Proposed)	B	From Leg	3.00 -6.00 0.00	0.0000	135.00	No Ice 1/2" Ice	2.87 3.18	3.73 4.10	0.02 0.04
APL866513-42T0 (Verizon - Proposed)	C	From Leg	3.00 6.00 0.00	0.0000	135.00	No Ice 1/2" Ice	4.29 4.67	3.73 4.10	0.02 0.05
BXA-70063/6CF (Verizon - Proposed)	C	From Leg	3.00 0.00 0.00	0.0000	135.00	No Ice 1/2" Ice	7.73 8.27	3.76 4.19	0.02 0.06
APX18-206516L-T0 (Verizon - Proposed)	C	From Leg	3.00 -4.00 0.00	0.0000	135.00	No Ice 1/2" Ice	3.51 3.85	2.00 2.33	0.02 0.04
APL866513-42T0 (Verizon - Proposed)	C	From Leg	3.00 -6.00	0.0000	135.00	No Ice 1/2" Ice	4.29 4.67	3.73 4.10	0.02 0.05

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	Client Verizon Wireless							Designed by TJL

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C <sub>AA</sub> Front ft <sup>2</sup>	C <sub>AA</sub> Side ft <sup>2</sup>	Weight K
3' Side Mount Standoff	A	From Leg	0.00 1.50 0.00 0.00	0.0000	178.00	No Ice 1/2" Ice	2.64 3.69	2.64 3.69
3' Side Mount Standoff	B	From Leg	0.00 1.50 0.00 0.00	0.0000	178.00	No Ice 1/2" Ice	2.64 3.69	2.64 3.69
3' Side Mount Standoff	C	From Leg	0.00 1.50 0.00 0.00	0.0000	178.00	No Ice 1/2" Ice	2.64 3.69	2.64 3.69
2 Bay Dipole	C	From Leg	3.00 0.00 0.00	0.0000	185.00	No Ice 1/2" Ice	2.66 4.44	2.66 4.44
2" Dia 10' Omni	A	From Leg	3.00 0.00 0.00	0.0000	185.00	No Ice 1/2" Ice	2.00 3.03	2.00 3.03
2" Dia 10' Omni	B	From Leg	3.00 0.00 0.00	0.0000	185.00	No Ice 1/2" Ice	2.00 3.03	2.00 3.03
2" Dia 10' Omni	C	None		0.0000	185.00	No Ice 1/2" Ice	2.00 3.03	2.00 3.03
3' Side Mount Standoff	A	From Leg	1.50 0.00 0.00	0.0000	150.00	No Ice 1/2" Ice	2.64 3.69	2.64 3.69
3' Side Mount Standoff	B	From Leg	1.50 0.00 0.00	0.0000	150.00	No Ice 1/2" Ice	2.64 3.69	2.64 3.69
3' Side Mount Standoff	C	From Leg	1.50 0.00 0.00	0.0000	150.00	No Ice 1/2" Ice	2.64 3.69	2.64 3.69
2" Dia 10' Omni	B	From Leg	3.00 0.00 0.00	0.0000	155.00	No Ice 1/2" Ice	2.00 3.03	2.00 3.03
2' Side Mount Standoff	C	From Leg	1.00 0.00 0.00	0.0000	140.00	No Ice 1/2" Ice	2.10 4.30	2.10 4.30
2" Dia 8' Omni	C	From Leg	2.00 0.00 0.00	0.0000	144.00	No Ice 1/2" Ice	2.00 3.03	2.00 3.03
2" Dia 8' Omni	B	From Leg	2.00 0.00 0.00	0.0000	104.00	No Ice 1/2" Ice	2.00 3.03	2.00 3.03
2' Side Mount Standoff	B	From Leg	1.00 0.00 0.00	0.0000	100.00	No Ice 1/2" Ice	2.10 4.30	2.10 4.30
Pirod 13' KD T-Frame	A	From Leg	2.00 0.00 0.00	0.0000	135.00	No Ice 1/2" Ice	11.07 15.53	11.07 15.53
Pirod 13' KD T-Frame	B	From Leg	2.00 0.00 0.00	0.0000	135.00	No Ice 1/2" Ice	11.07 15.53	11.07 15.53
Pirod 13' KD T-Frame	C	From Leg	2.00 0.00 0.00	0.0000	135.00	No Ice 1/2" Ice	11.07 15.53	11.07 15.53

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## Tower Pressures - No Ice

$$G_H = 1.121$$

Section Elevation ft	z ft	K <sub>Z</sub>	q <sub>z</sub> psf	A <sub>G</sub> ft <sup>2</sup>	F a c e	A <sub>F</sub> ft <sup>2</sup>	A <sub>R</sub> ft <sup>2</sup>	A <sub>leg</sub> ft <sup>2</sup>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
T1 180.00-160.00	170.00	1.597	30	134.358	A B C	10.531 10.531 9.867	7.917 7.917 16.050	7.917	42.91	0.000	0.000
T2 160.00-140.00	150.00	1.541	29	134.758	A B C	9.479 9.479 8.815	7.917 7.917 16.975	7.917	45.51	0.000	0.000
T3 140.00-120.00	130.00	1.48	27	155.998	A B C	11.721 11.721 11.988	24.449 24.449 21.433	9.599	30.70	0.000	0.000
T4 120.00-113.33	116.67	1.434	27	60.927	A B C	3.267 3.267 3.433	9.799 9.799 7.144	3.200	28.72	0.000	0.000
T5 113.33-106.67	110.00	1.411	26	65.466	A B C	6.382 6.382 6.684	9.800 9.800 7.144	3.200	24.49	0.000	0.000
T6 106.67-100.00	103.33	1.386	26	69.999	A B C	4.588 4.588 4.785	9.800 9.800 7.144	3.200	24.49	0.000	0.000
T7 100.00-80.00	90.00	1.332	25	237.841	A B C	15.219 15.219 15.724	31.486 31.486 24.486	11.686	23.14	0.000	0.000
T8 80.00-60.00	70.00	1.24	23	278.841	A B C	17.581 17.581 18.068	31.488 31.488 24.488	11.688	22.24	0.000	0.000
T9 60.00-40.00	50.00	1.126	21	321.509	A B C	17.388 17.388 17.804	34.825 34.825 27.825	15.025	22.24	0.000	0.000
T10 40.00-20.00	30.00	1	18	362.210	A B C	19.195 19.195 19.597	34.827 34.827 27.827	15.027	26.82	0.000	0.000
T11 20.00-0.00	10.00	1	18	404.797	A B C	25.008 25.008 25.199	30.456 30.456 27.536	18.575	32.93	0.000	0.000
										27.82	0.000
										31.69	0.000
										33.49	0.000
										35.22	0.000
											0.000

## Tower Pressure - With Ice

$$G_H = 1.121$$

Section Elevation ft	z ft	K <sub>Z</sub>	q <sub>z</sub> psf	t <sub>Z</sub> in	A <sub>G</sub> ft <sup>2</sup>	F a c e	A <sub>F</sub> ft <sup>2</sup>	A <sub>R</sub> ft <sup>2</sup>	A <sub>leg</sub> ft <sup>2</sup>	Leg %	C <sub>A</sub> A <sub>A</sub> In Face ft <sup>2</sup>	C <sub>A</sub> A <sub>A</sub> Out Face ft <sup>2</sup>
T1 180.00-160.00	170.00	1.597	22	0.5000	136.025	A B C	10.531 10.531 9.323	17.958 17.958 31.973	11.250	39.49	0.000	0.000
T2 160.00-140.00	150.00	1.541	22	0.5000	136.425	A B C	9.479 9.479 8.266	17.445 17.445 33.195	11.250	41.78	0.000	0.000





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	Client	Verizon Wireless	Designed by TJL

### Tower Forces - No Ice - Wind 60 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w plf	Ctrl. Face
T1 180.00- 160.00	0.05	0.54	A	0.137	2.819	0.58	0.8	1	13.014	1.51	75.25	C
			B	0.137	2.819	0.58	0.8	1	13.014			
			C	0.193	2.62	0.589	0.8	1	17.347			
T2 160.00- 140.00	0.05	0.51	A	0.129	2.85	0.578	0.8	1	12.163	1.43	71.48	C
			B	0.129	2.85	0.578	0.8	1	12.163			
			C	0.191	2.625	0.589	0.8	1	17.045			
T3 140.00- 120.00	0.25	0.93	A	0.232	2.493	0.597	0.8	1	23.983	1.83	91.70	B
			B	0.232	2.493	0.597	0.8	1	23.983			
			C	0.214	2.549	0.593	0.8	1	22.309			
T4 120.00- 113.33	0.11	0.32	A	0.214	2.548	0.593	0.8	1	8.429	0.64	95.83	B
			B	0.214	2.548	0.593	0.8	1	8.429			
			C	0.174	2.687	0.585	0.8	1	6.928			
T5 113.33- 106.67	0.11	0.48	A	0.247	2.446	0.601	0.8	1	10.997	0.79	117.99	B
			B	0.247	2.446	0.601	0.8	1	10.997			
			C	0.211	2.559	0.593	0.8	1	9.582			
T6 106.67- 100.00	0.11	0.39	A	0.206	2.578	0.592	0.8	1	9.467	0.70	105.15	B
			B	0.206	2.578	0.592	0.8	1	9.467			
			C	0.17	2.698	0.585	0.8	1	8.006			
T7 100.00- 80.00	0.33	1.38	A	0.196	2.608	0.59	0.8	1	30.742	2.21	110.70	B
			B	0.196	2.608	0.59	0.8	1	30.742			
			C	0.169	2.703	0.585	0.8	1	26.893			
T8 80.00- 60.00	0.33	1.49	A	0.176	2.678	0.586	0.8	1	32.510	2.24	111.89	B
			B	0.176	2.678	0.586	0.8	1	32.510			
			C	0.153	2.762	0.582	0.8	1	28.704			
T9 60.00- 40.00	0.33	1.76	A	0.162	2.726	0.583	0.8	1	34.229	2.18	108.93	B
			B	0.162	2.726	0.583	0.8	1	34.229			
			C	0.142	2.801	0.58	0.8	1	30.389			
T10 40.00- 20.00	0.33	1.84	A	0.149	2.775	0.581	0.8	1	35.602	2.05	102.40	B
			B	0.149	2.775	0.581	0.8	1	35.602			
			C	0.131	2.843	0.579	0.8	1	31.782			
T11 20.00- 0.00	0.20	2.46	A	0.137	2.82	0.58	0.8	1	37.658	2.20	110.07	B
			B	0.137	2.82	0.58	0.8	1	37.658			
			C	0.13	2.845	0.579	0.8	1	36.093			
Sum Weight:	2.19	12.11						OTM	1490.52 kip-ft	17.77		

### Tower Forces - No Ice - Wind 90 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w plf	Ctrl. Face
T1 180.00- 160.00	0.05	0.54	A	0.137	2.819	0.58	0.85	1	13.540	1.55	77.39	C
			B	0.137	2.819	0.58	0.85	1	13.540			
			C	0.193	2.62	0.589	0.85	1	17.840			
T2 160.00- 140.00	0.05	0.51	A	0.129	2.85	0.578	0.85	1	12.637	1.47	73.33	C
			B	0.129	2.85	0.578	0.85	1	12.637			
			C	0.191	2.625	0.589	0.85	1	17.486			
T3 140.00-	0.25	0.93	A	0.232	2.493	0.597	0.85	1	24.569	1.88	93.94	B



**RISA Tower**

**Centek Engineering Inc.**  
63-2 North Branford Road  
Branford, CT 06405  
Phone: 203.488.0580  
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Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
T8 80.00- 60.00	0.83	2.27	A B C	0.244 0.244 0.226	2.457 2.457 2.51	0.6 0.6 0.596	1 1 1	1 1 1	47.758 47.758 44.827	2.29	114.28	B
T9 60.00- 40.00	0.83	2.55	A B C	0.218 0.218 0.203	2.537 2.537 2.587	0.594 0.594 0.591	1 1 1	1 1 1	48.670 48.670 45.722	2.18	109.24	B
T10 40.00- 20.00	0.83	2.69	A B C	0.2 0.2 0.187	2.595 2.595 2.641	0.59 0.59 0.588	1 1 1	1 1 1	50.647 50.647 47.733	2.07	103.27	B
T11 20.00- 0.00	0.52	3.51	A B C	0.175 0.175 0.174	2.68 2.68 2.686	0.586 0.586 0.585	1 1 1	1 1 1	51.959 51.959 51.561	2.19	109.40	B
Sum Weight:	5.56	18.49						OTM	1560.61 kip-ft	18.28		

**Tower Forces - With Ice - Wind 60 To Face**

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
T1 180.00- 160.00	0.13	1.04	A B C	0.209 0.209 0.304	2.565 2.565 2.287	0.592 0.592 0.617	0.8 0.8 0.8	1 1 1	19.063 19.063 27.186	1.56	78.01	C
T2 160.00- 140.00	0.14	0.97	A B C	0.197 0.197 0.304	2.605 2.605 2.286	0.59 0.59 0.617	0.8 0.8 0.8	1 1 1	17.873 17.873 27.097	1.50	75.00	C
T3 140.00- 120.00	0.65	1.51	A B C	0.328 0.328 0.325	2.224 2.224 2.231	0.625 0.625 0.624	0.8 0.8 0.8	1 1 1	34.274 34.274 33.964	1.77	88.59	B
T4 120.00- 113.33	0.27	0.49	A B C	0.306 0.306 0.267	2.281 2.281 2.389	0.618 0.618 0.606	0.8 0.8 0.8	1 1 1	12.168 12.168 10.562	0.63	93.85	B
T5 113.33- 106.67	0.27	0.76	A B C	0.34 0.34 0.306	2.194 2.194 2.279	0.629 0.629 0.618	0.8 0.8 0.8	1 1 1	15.161 15.161 13.648	0.74	110.60	B
T6 106.67- 100.00	0.27	0.60	A B C	0.287 0.287 0.254	2.33 2.33 2.426	0.612 0.612 0.603	0.8 0.8 0.8	1 1 1	13.230 13.230 11.687	0.67	100.67	B
T7 100.00- 80.00	0.83	2.09	A B C	0.271 0.271 0.251	2.375 2.375 2.434	0.608 0.608 0.602	0.8 0.8 0.8	1 1 1	42.276 42.276 39.195	2.10	105.07	B
T8 80.00- 60.00	0.83	2.27	A B C	0.244 0.244 0.226	2.457 2.457 2.51	0.6 0.6 0.596	0.8 0.8 0.8	1 1 1	44.381 44.381 41.375	2.12	106.20	B
T9 60.00- 40.00	0.83	2.55	A B C	0.218 0.218 0.203	2.537 2.537 2.587	0.594 0.594 0.591	0.8 0.8 0.8	1 1 1	45.311 45.311 42.300	2.03	101.70	B
T10 40.00- 20.00	0.83	2.69	A B C	0.2 0.2 0.187	2.595 2.595 2.641	0.59 0.59 0.588	0.8 0.8 0.8	1 1 1	46.923 46.923 43.948	1.91	95.67	B
T11 20.00- 0.00	0.52	3.51	A B C	0.175 0.175 0.174	2.68 2.68 2.686	0.586 0.586 0.585	0.8 0.8 0.8	1 1 1	47.035 47.035 46.628	1.98	99.04	B
Sum Weight:	5.56	18.49						OTM	1460.74	17.02		

**RISATower**

**Centeck Engineering Inc.**  
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Project	180' Self-Support Lattice 1192 Wolcott Road., Wolcott, CT	17 of 31
Client	Verizon Wireless	Date 16:40:36 01/24/11
		Designed by TJL

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
									ft <sup>2</sup>	K	plf	
									kip-ft			

**Tower Forces - With Ice - Wind 90 To Face**

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
T1 180.00-160.00	0.13	1.04	A B C	0.209 0.209 0.304	2.565 2.565 2.287	0.592 0.592 0.617	0.85 0.85 0.85	1 1 1	19.589 19.589 27.652	1.59	79.35	C
T2 160.00-140.00	0.14	0.97	A B C	0.197 0.197 0.304	2.605 2.605 2.286	0.59 0.59 0.617	0.85 0.85 0.85	1 1 1	18.347 18.347 27.510	1.52	76.14	C
T3 140.00-120.00	0.65	1.51	A B C	0.328 0.328 0.325	2.224 2.224 2.231	0.625 0.625 0.624	0.85 0.85 0.85	1 1 1	34.827 34.827 34.520	1.80	90.02	B
T4 120.00-113.33	0.27	0.49	A B C	0.306 0.306 0.267	2.281 2.281 2.389	0.618 0.618 0.606	0.85 0.85 0.85	1 1 1	12.321 12.321 10.723	0.63	95.03	B
T5 113.33-106.67	0.27	0.76	A B C	0.34 0.34 0.306	2.194 2.194 2.279	0.629 0.629 0.618	0.85 0.85 0.85	1 1 1	15.461 15.461 13.963	0.75	112.79	B
T6 106.67-100.00	0.27	0.60	A B C	0.287 0.287 0.254	2.33 2.33 2.426	0.612 0.612 0.603	0.85 0.85 0.85	1 1 1	13.447 13.447 11.914	0.68	102.32	B
T7 100.00-80.00	0.83	2.09	A B C	0.271 0.271 0.251	2.375 2.375 2.434	0.608 0.608 0.602	0.85 0.85 0.85	1 1 1	43.001 43.001 39.939	2.14	106.87	B
T8 80.00-60.00	0.83	2.27	A B C	0.244 0.244 0.226	2.457 2.457 2.51	0.6 0.6 0.596	0.85 0.85 0.85	1 1 1	45.225 45.225 42.238	2.16	108.22	B
T9 60.00-40.00	0.83	2.55	A B C	0.218 0.218 0.203	2.537 2.537 2.587	0.594 0.594 0.591	0.85 0.85 0.85	1 1 1	46.151 46.151 43.155	2.07	103.59	B
T10 40.00-20.00	0.83	2.69	A B C	0.2 0.2 0.187	2.595 2.595 2.641	0.59 0.59 0.588	0.85 0.85 0.85	1 1 1	47.854 47.854 44.894	1.95	97.57	B
T11 20.00-0.00	0.52	3.51	A B C	0.175 0.175 0.174	2.68 2.68 2.686	0.586 0.586 0.585	0.85 0.85 0.85	1 1 1	48.266 48.266 47.861	2.03	101.63	B
Sum Weight:	5.56	18.49						OTM	1485.70 kip-ft	17.34		

**Tower Forces - Service - Wind Normal To Face**

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
T1 180.00-	0.05	0.54	A	0.137	2.819	0.58	1	1	15.120	0.58	29.00	C



**RISATower**

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Project	180' Self-Support Lattice 1192 Wolcott Road., Wolcott, CT	Date
Client	Verizon Wireless	Designed by TJL

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
T6 106.67-100.00	0.11	0.39	A B C	0.206 0.206 0.17	2.578 2.578 2.698	0.592 0.592 0.585	0.8 0.8 0.8	1 1 1	9.467 9.467 8.006	0.24	36.38	B
T7 100.00-80.00	0.33	1.38	A B C	0.196 0.196 0.169	2.608 2.608 2.703	0.59 0.59 0.585	0.8 0.8 0.8	1 1 1	30.742 30.742 26.893	0.77	38.31	B
T8 80.00-60.00	0.33	1.49	A B C	0.176 0.176 0.153	2.678 2.678 2.762	0.586 0.586 0.582	0.8 0.8 0.8	1 1 1	32.510 32.510 28.704	0.77	38.72	B
T9 60.00-40.00	0.33	1.76	A B C	0.162 0.162 0.142	2.726 2.726 2.801	0.583 0.583 0.58	0.8 0.8 0.8	1 1 1	34.229 34.229 30.389	0.75	37.69	B
T10 40.00-20.00	0.33	1.84	A B C	0.149 0.149 0.131	2.775 2.775 2.843	0.581 0.581 0.579	0.8 0.8 0.8	1 1 1	35.602 35.602 31.782	0.71	35.43	B
T11 20.00-0.00	0.20	2.46	A B C	0.137 0.137 0.13	2.82 2.82 2.845	0.58 0.58 0.579	0.8 0.8 0.8	1 1 1	37.658 37.658 36.093	0.76	38.09	B
Sum Weight:	2.19	12.11						OTM	515.75 kip-ft	6.15		

**Tower Forces - Service - Wind 90 To Face**

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
T1 180.00-160.00	0.05	0.54	A B C	0.137 0.137 0.193	2.819 2.819 2.62	0.58 0.58 0.589	0.85 0.85 0.85	1 1 1	13.540 13.540 17.840	0.54	26.78	C
T2 160.00-140.00	0.05	0.51	A B C	0.129 0.129 0.191	2.85 2.85 2.625	0.578 0.578 0.589	0.85 0.85 0.85	1 1 1	12.637 12.637 17.486	0.51	25.37	C
T3 140.00-120.00	0.25	0.93	A B C	0.232 0.232 0.214	2.493 2.493 2.549	0.597 0.597 0.593	0.85 0.85 0.85	1 1 1	24.569 24.569 22.908	0.65	32.50	B
T4 120.00-113.33	0.11	0.32	A B C	0.214 0.214 0.174	2.548 2.548 2.687	0.593 0.593 0.585	0.85 0.85 0.85	1 1 1	8.592 8.592 7.100	0.23	33.80	B
T5 113.33-106.67	0.11	0.48	A B C	0.247 0.247 0.211	2.446 2.446 2.559	0.601 0.601 0.593	0.85 0.85 0.85	1 1 1	11.316 11.316 9.916	0.28	42.01	B
T6 106.67-100.00	0.11	0.39	A B C	0.206 0.206 0.17	2.578 2.578 2.698	0.592 0.592 0.585	0.85 0.85 0.85	1 1 1	9.697 9.697 8.246	0.25	37.26	B
T7 100.00-80.00	0.33	1.38	A B C	0.196 0.196 0.169	2.608 2.608 2.703	0.59 0.59 0.585	0.85 0.85 0.85	1 1 1	31.503 31.503 27.680	0.79	39.25	B
T8 80.00-60.00	0.33	1.49	A B C	0.176 0.176 0.153	2.678 2.678 2.762	0.586 0.586 0.582	0.85 0.85 0.85	1 1 1	33.389 33.389 29.607	0.80	39.76	B
T9 60.00-40.00	0.33	1.76	A B C	0.162 0.162 0.142	2.726 2.726 2.801	0.583 0.583 0.58	0.85 0.85 0.85	1 1 1	35.099 35.099 31.279	0.77	38.65	B
T10 40.00-20.00	0.33	1.84	A B	0.149 0.149	2.775 2.775	0.581 0.581	0.85 0.85	1	36.562 36.562	0.73	36.39	B

<b>RISATower</b>  Centek Engineering Inc. 63-2 North Branford Road Branford, CT 06405 Phone: 203.488.0580 FAX: 203.488.8587	Job 11001.CO4 ~ Wolcott North	Page 20 of 31
	Project 180' Self-Support Lattice 1192 Wolcott Road., Wolcott, CT	Date 16:40:36 01/24/11
	Client Verizon Wireless	Designed by TJL

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F	w	Ctrl Face
T11 20.00-0.00	0.20	2.46	C A B C	0.131 0.137 0.137 0.13	2.843 2.82 2.82 2.845	0.579 0.58 0.58 0.579	0.85 0.85 0.85 0.85	1 1 1 OTM	32.762 38.909 38.909 37.353 529.13 kip-ft	0.79	39.35	B
Sum Weight:	2.19	12.11								6.32		

### Force Totals

Load Case	Vertical Forces K	Sum of Forces X K	Sum of Forces Z K	Sum of Overturning Moments, M <sub>x</sub> kip-ft	Sum of Overturning Moments, M <sub>z</sub> kip-ft	Sum of Torques kip-ft
Leg Weight	5.27					
Bracing Weight	6.84					
Total Member Self-Weight	12.11			-7.55	3.10	
Total Weight	15.69			-7.55	3.10	
Wind 0 deg - No Ice		0.04	-23.26	-2164.88	-2.56	-7.82
Wind 90 deg - No Ice		21.87	-0.04	-13.21	-2043.59	-16.78
Wind 180 deg - No Ice		-0.04	21.36	1995.06	8.77	7.02
Member Ice	6.38					
Total Weight Ice	26.34			-18.15	8.40	
Wind 0 deg - Ice		0.03	-21.87	-2094.42	3.92	-9.39
Wind 90 deg - Ice		20.96	-0.03	-22.62	-1997.26	-14.65
Wind 180 deg - Ice		-0.03	20.61	1958.25	12.87	8.70
Total Weight	15.69			-7.55	3.10	
Wind 0 deg - Service		0.01	-8.05	-745.98	-1.89	-2.71
Wind 90 deg - Service		7.57	-0.01	-1.46	-708.13	-5.81
Wind 180 deg - Service		-0.01	7.39	693.45	2.03	2.43

### Load Combinations

Comb. No.	Description
1	Dead Only
2	Dead+Wind 0 deg - No Ice
3	Dead+Wind 90 deg - No Ice
4	Dead+Wind 180 deg - No Ice
5	Dead+Ice+Temp
6	Dead+Wind 0 deg+Ice+Temp
7	Dead+Wind 90 deg+Ice+Temp
8	Dead+Wind 180 deg+Ice+Temp
9	Dead+Wind 0 deg - Service
10	Dead+Wind 90 deg - Service
11	Dead+Wind 180 deg - Service

### Maximum Member Forces

# RISATower

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Project	180' Self-Support Lattice 1192 Wolcott Road., Wolcott, CT	Date
Client	Verizon Wireless	Designed by TJL

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
T1	180 - 160	Leg	Max Tension	8	4.13	0.00	-0.01
			Max. Compression	6	-5.03	-0.01	0.01
			Max. Mx	7	-0.55	0.09	0.00
			Max. My	6	0.01	-0.00	-0.09
			Max. Vy	7	-0.18	0.00	0.00
			Max. Vx	8	-0.19	0.00	0.00
			Diagonal	7	0.88	0.00	0.00
		Top Girt	Max Tension	7	-0.88	0.00	0.00
			Max. Compression	7	0.36	0.01	-0.00
			Max. Mx	6	-0.06	0.01	0.00
			Max. My	7	0.01	0.01	-0.00
			Max. Vy	6	0.00	0.00	0.00
			Max. Vx	6	0.04	0.00	0.00
			Max. Compression	8	-0.07	0.00	0.00
			Max. Mx	5	-0.01	-0.02	0.00
T2	160 - 140	Leg	Max. My	6	-0.04	0.00	-0.00
			Max. Vy	5	0.01	0.00	0.00
			Max. Vx	6	0.00	0.00	0.00
			Max Tension	8	14.19	-0.00	-0.00
			Max. Compression	6	-16.28	0.06	0.01
		Diagonal	Max. Mx	6	-16.28	0.06	0.01
			Max. My	7	-0.55	-0.00	-0.06
			Max. Vy	6	-0.06	0.06	0.01
			Max. Vx	6	0.07	-0.00	0.03
			Max Tension	7	1.71	0.00	0.00
T3	140 - 120	Leg	Max. Compression	7	-1.74	0.00	0.00
			Max. Mx	6	1.47	0.01	0.00
			Max. My	6	-1.32	0.00	0.00
			Max. Vy	6	-0.01	0.01	0.00
			Max. Vx	6	-0.00	0.00	0.00
			Max Tension	8	27.17	-0.07	-0.00
			Max. Compression	6	-32.58	0.02	0.01
		Diagonal	Max. Mx	2	-26.56	0.08	0.00
			Max. My	3	-1.28	-0.01	0.16
			Max. Vy	4	-0.86	-0.04	-0.00
			Max. Vx	3	0.85	-0.00	0.02
			Max Tension	7	2.38	0.00	0.00
			Max. Compression	7	-2.38	0.00	0.00
			Max. Mx	7	0.90	0.03	-0.00
			Max. My	8	-2.15	0.01	-0.01
T4	120 - 113.334	Leg	Max. Vy	7	0.01	0.03	-0.00
			Max. Vx	8	0.00	0.00	0.00
			Max Tension	4	0.38	0.00	0.00
			Max. Compression	2	-0.36	0.00	0.00
			Max. Mx	5	0.01	-0.02	0.00
			Max. My	8	-0.17	0.00	0.00
			Max. Vy	5	0.01	0.00	0.00
		Diagonal	Max. Vx	8	-0.00	0.00	0.00
			Max Tension	8	31.08	-0.04	-0.01
			Max. Compression	6	-37.07	0.10	0.02
			Max. Mx	2	-35.62	0.11	0.01
			Max. My	3	-1.36	-0.01	0.16
			Max. Vy	4	0.04	-0.10	-0.01
			Max. Vx	3	0.07	-0.01	0.16
T5	113.334 -	Leg	Max Tension	8	2.43	0.00	0.00
			Max. Compression	6	-2.64	0.00	0.00
			Max. Mx	6	1.69	0.03	0.00
			Max. My	8	1.99	0.02	-0.00
			Max. Vy	6	-0.01	0.03	0.00
			Max. Vx	8	0.00	0.00	0.00
			Max Tension	4	35.65	-0.10	-0.01

<b>RISATower</b>  Centek Engineering Inc. 63-2 North Branford Road Branford, CT 06405 Phone: 203.488.0580 FAX: 203.488.8587	Job	11001.CO4 ~ Wolcott North	Page
	Project	180' Self-Support Lattice 1192 Wolcott Road., Wolcott, CT	Date
	Client	Verizon Wireless	Designed by TJL

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
	106.667						
T6	106.667 - 100.001	Leg					
T7	100.001 - 80.0007	Leg	Max Tension	4	54.07	-0.11	-0.01
T8	80.0007 - 60.0007	Leg					
T9	60.0007 - 40.0007	Leg	Max Tension	4	78.68	-0.21	-0.02
			Max. Compression	6	-93.30	-0.11	0.02
			Max. Mx	8	75.16	-0.61	-0.02

# RISATower

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Job	11001.CO4 ~ Wolcott North	Page
Project	180' Self-Support Lattice 1192 Wolcott Road., Wolcott, CT	23 of 31
Client	Verizon Wireless	Date 16:40:36 01/24/11
		Designed by TJL

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
T10	40.0007 - 20.0007	Leg	Diagonal	Max. My	3	-3.76	-0.03
				Max. Vy	8	0.12	-0.61
				Max. Vx	3	0.11	-0.03
				Max Tension	8	3.82	0.00
				Max. Compression	2	-3.93	0.00
				Max. Mx	8	2.49	0.09
				Max. My	8	-3.56	0.06
				Max. Vy	8	0.04	-0.09
			Diagonal	Max. Vx	8	0.00	0.00
				Max Tension	4	90.98	-0.16
				Max. Compression	6	-108.11	-0.29
				Max. Mx	8	86.25	-0.99
				Max. My	3	-4.56	-0.04
				Max. Vy	8	0.18	-0.99
				Max. Vx	3	0.11	-0.04
				Max Tension	8	4.15	0.00
T11	20.0007 - 0	Leg	Diagonal	Max. Compression	2	-4.13	0.00
				Max. Mx	8	2.40	0.11
				Max. My	8	-3.88	0.08
				Max. Vy	8	0.04	0.11
				Max. Vx	8	0.00	0.00
				Max Tension	4	102.92	-0.34
				Max. Compression	6	-122.68	-0.00
				Max. Mx	6	-114.45	1.02
			Diagonal	Max. My	3	-5.35	-0.04
				Max. Vy	8	-0.20	-0.99
				Max. Vx	3	0.16	-0.04
				Max Tension	8	4.94	0.00
				Max. Compression	2	-4.78	0.00
				Max. Mx	8	2.20	0.23
				Max. My	8	-4.61	0.16
				Max. Vy	8	0.06	0.23
				Max. Vx	8	0.00	0.00

## Maximum Reactions

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Leg C	Max. Vert	8	64.04	4.12	-4.10
	Max. H <sub>x</sub>	4	61.23	5.07	-4.76
	Max. H <sub>z</sub>	7	-88.37	-10.04	5.45
	Min. Vert	3	-93.73	-9.51	5.12
	Min. H <sub>x</sub>	7	-88.37	-10.04	5.45
	Min. H <sub>z</sub>	4	61.23	5.07	-4.76
	Max. Vert	7	104.67	-9.07	-4.87
	Max. H <sub>x</sub>	6	-49.85	5.65	4.43
Leg B	Max. H <sub>z</sub>	6	-49.85	5.65	4.43
	Min. Vert	2	-54.95	4.96	4.32
	Min. H <sub>x</sub>	3	103.45	-10.27	-5.51
	Min. H <sub>z</sub>	3	103.45	-10.27	-5.51
	Max. Vert	2	125.83	-0.22	14.23
	Max. H <sub>x</sub>	8	-100.49	0.24	-12.85
	Max. H <sub>z</sub>	2	125.83	-0.22	14.23
	Min. Vert	4	-105.91	0.20	-12.20
Leg A	Min. H <sub>x</sub>	3	5.97	-2.09	0.43

<b>RISA Tower</b>	<b>Job</b> 11001.CO4 ~ Wolcott North	<b>Page</b> 24 of 31
<b>Centek Engineering Inc.</b> 63-2 North Branford Road Branford, CT 06405 Phone: 203.488.0580 FAX: 203.488.8587	<b>Project</b> 180' Self-Support Lattice 1192 Wolcott Road., Wolcott, CT	<b>Date</b> 16:40:36 01/24/11
	<b>Client</b> Verizon Wireless	<b>Designed by</b> TJL

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Min. H <sub>z</sub>	8		-100.49	0.24	-12.85

### Tower Mast Reaction Summary

Load Combination	Vertical	Shear <sub>x</sub>	Shear <sub>z</sub>	Overturning Moment, M <sub>x</sub> kip-ft	Overturning Moment, M <sub>z</sub> kip-ft	Torque kip-ft
	K	K	K			
Dead Only	15.69	0.00	0.00	-7.55	3.10	-0.00
Dead+Wind 0 deg - No Ice	15.69	0.04	-23.26	-2170.29	-2.54	-7.84
Dead+Wind 90 deg - No Ice	15.69	21.87	-0.04	-13.28	-2048.72	-16.81
Dead+Wind 180 deg - No Ice	15.69	-0.04	21.36	2000.08	8.81	7.04
Dead+Ice+Temp	26.34	0.00	0.00	-18.19	8.43	-0.00
Dead+Wind 0 deg+Ice+Temp	26.34	0.03	-21.87	-2103.22	4.00	-9.44
Dead+Wind 90 deg+Ice+Temp	26.34	20.96	-0.03	-22.74	-2005.66	-14.73
Dead+Wind 180 deg+Ice+Temp	26.34	-0.03	20.61	1966.51	12.96	8.74
Dead+Wind 0 deg - Service	15.69	0.01	-8.05	-755.93	1.15	-2.71
Dead+Wind 90 deg - Service	15.69	7.57	-0.01	-9.53	-706.87	-5.82
Dead+Wind 180 deg - Service	15.69	-0.01	7.39	687.13	5.08	2.44

### Solution Summary

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
1	0.00	-15.69	0.00	0.00	15.69	0.00	0.000%
2	0.04	-15.69	-23.26	-0.04	15.69	23.26	0.000%
3	21.87	-15.69	-0.04	-21.87	15.69	0.04	0.000%
4	-0.04	-15.69	21.36	0.04	15.69	-21.36	0.000%
5	0.00	-26.34	0.00	0.00	26.34	0.00	0.000%
6	0.03	-26.34	-21.87	-0.03	26.34	21.87	0.000%
7	20.96	-26.34	-0.03	-20.96	26.34	0.03	0.000%
8	-0.03	-26.34	20.61	0.03	26.34	-20.61	0.000%
9	0.01	-15.69	-8.05	-0.01	15.69	8.05	0.000%
10	7.57	-15.69	-0.01	-7.57	15.69	0.01	0.000%
11	-0.01	-15.69	7.39	0.01	15.69	-7.39	0.000%

### Non-Linear Convergence Results

Load Combination	Converged?	Number of Cycles	Displacement Tolerance	Force Tolerance
1	Yes	4	0.00000001	0.00000001
2	Yes	4	0.00000001	0.00000197
3	Yes	4	0.00000001	0.00000267
4	Yes	4	0.00000001	0.00000302
5	Yes	4	0.00000001	0.00000001
6	Yes	4	0.00000001	0.00000488
7	Yes	4	0.00000001	0.00000365
8	Yes	4	0.00000001	0.00000228
9	Yes	4	0.00000001	0.00000001
10	Yes	4	0.00000001	0.00000001

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Yes

4

0.0000001

0.0000001

## Maximum Tower Deflections - Service Wind

Section No.	Elevation	Horz. Deflection	Gov. Load Comb.	Tilt	Twist
	ft	in		°	°
T1	180 - 160	5.941	9	0.2915	0.0173
T2	160 - 140	4.719	9	0.2845	0.0155
T3	140 - 120	3.563	9	0.2508	0.0120
T4	120 - 113.334	2.574	9	0.2090	0.0127
T5	113.334 - 106.667	2.287	9	0.1959	0.0126
T6	106.667 - 100.001	2.015	9	0.1815	0.0123
T7	100.001 - 80.0007	1.768	9	0.1664	0.0118
T8	80.0007 - 60.0007	1.125	9	0.1296	0.0099
T9	60.0007 - 40.0007	0.640	9	0.0898	0.0071
T10	40.0007 - 20.0007	0.301	9	0.0612	0.0046
T11	20.0007 - 0	0.083	9	0.0315	0.0018

## Critical Deflections and Radius of Curvature - Service Wind

Elevation	Appurtenance	Gov. Load Comb.	Deflection	Tilt	Twist	Radius of Curvature ft
			in	°	°	
185.00	2 Bay Dipole	9	5.941	0.2915	0.0173	357791
178.00	3' Side Mount Standoff	9	5.818	0.2914	0.0172	357791
155.00	2" Dia 10' Omni	9	4.420	0.2784	0.0147	56139
150.00	3' Side Mount Standoff	9	4.126	0.2704	0.0138	40226
144.00	2" Dia 8' Omni	9	3.784	0.2590	0.0127	30023
140.00	2' Side Mount Standoff	9	3.563	0.2508	0.0120	26371
135.00	APL868013-42T0	9	3.298	0.2402	0.0118	25125
104.00	2" Dia 8' Omni	9	1.914	0.1754	0.0121	22645
100.00	2' Side Mount Standoff	9	1.768	0.1664	0.0118	33049

## Maximum Tower Deflections - Design Wind

Section No.	Elevation	Horz. Deflection	Gov. Load Comb.	Tilt	Twist
	ft	in		°	°
T1	180 - 160	17.090	2	0.8435	0.0601
T2	160 - 140	13.567	2	0.8213	0.0532
T3	140 - 120	10.237	2	0.7216	0.0416
T4	120 - 113.334	7.393	2	0.6005	0.0367
T5	113.334 - 106.667	6.568	2	0.5627	0.0364
T6	106.667 - 100.001	5.787	2	0.5212	0.0355
T7	100.001 - 80.0007	5.078	2	0.4778	0.0342
T8	80.0007 - 60.0007	3.232	2	0.3721	0.0287
T9	60.0007 - 40.0007	1.838	2	0.2576	0.0205
T10	40.0007 - 20.0007	0.866	2	0.1755	0.0132
T11	20.0007 - 0	0.239	2	0.0903	0.0053

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### Critical Deflections and Radius of Curvature - Design Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
185.00	2 Bay Dipole	2	17.090	0.8435	0.0601	115239
178.00	3' Side Mount Standoff	2	16.735	0.8432	0.0595	115239
155.00	2" Dia 10' Omni	2	12.705	0.8026	0.0506	18178
150.00	3' Side Mount Standoff	2	11.858	0.7787	0.0477	13138
144.00	2" Dia 8' Omni	2	10.872	0.7456	0.0440	9861
140.00	2' Side Mount Standoff	2	10.237	0.7216	0.0416	8693
135.00	APL868013-42T0	2	9.473	0.6910	0.0387	8354
104.00	2" Dia 8' Omni	2	5.496	0.5036	0.0350	7828
100.00	2' Side Mount Standoff	2	5.078	0.4777	0.0342	11427

### Bolt Design Data

Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt K	Allowable Load K	Ratio Load Allowable	Allowable Ratio	Criteria	
										Member Bearing	Bolt Tension
T1	180	Diagonal	A325N	0.6250	1	0.88	4.08	0.216 ✓	1.333	Member Bearing	
T2	160	Leg	A325N	0.6250	4	1.40	13.50	0.104 ✓	1.333	Bolt Tension	
		Diagonal	A325N	0.6250	1	1.71	4.08	0.420 ✓	1.333	Member Bearing	
T3	140	Leg	A325N	0.6250	4	4.10	13.50	0.304 ✓	1.333	Bolt Tension	
		Diagonal	A325N	0.6250	1	2.38	6.12	0.389 ✓	1.333	Member Bearing	
T4	120	Leg	A325N	0.6250	4	7.77	13.50	0.576 ✓	1.333	Bolt Tension	
		Diagonal	A325N	0.6250	1	2.64	6.44	0.409 ✓	1.333	Bolt Shear	
T5	113.334	Diagonal	A325N	0.6250	1	2.75	6.44	0.427 ✓	1.333	Bolt Shear	
		Horizontal	A325N	0.5000	1	0.61	4.12	0.147 ✓	1.333	Bolt Shear	
T6	106.667	Diagonal	A325N	0.6250	1	2.65	6.12	0.433 ✓	1.333	Member Bearing	
T7	100.001	Leg	A325N	0.7500	4	11.24	19.44	0.578 ✓	1.333	Bolt Tension	
		Diagonal	A325N	0.6250	1	3.00	6.44	0.466 ✓	1.333	Bolt Shear	
T8	80.0007	Leg	A325N	0.8750	4	14.63	26.46	0.553 ✓	1.333	Bolt Tension	
		Diagonal	A325N	0.6250	1	3.12	6.12	0.510 ✓	1.333	Member Bearing	
T9	60.0007	Leg	A325N	0.8750	4	18.08	26.46	0.683 ✓	1.333	Bolt Tension	
		Diagonal	A325N	0.6250	1	3.82	6.12	0.625 ✓	1.333	Member Bearing	
T10	40.0007	Leg	A325N	0.8750	4	21.25	26.46	0.803 ✓	1.333	Bolt Tension	
		Diagonal	A325N	0.6250	1	4.15	6.12	0.678 ✓	1.333	Member Bearing	
T11	20.0007	Leg	A325N	1.0000	4	24.29	34.56	0.703 ✓	1.333	Bolt Tension	
		Diagonal	A325N	0.6250	1	4.94	6.44	0.767 ✓	1.333	Bolt Shear	

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**Compression Checks**
**Leg Design Data (Compression)**

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	F <sub>a</sub>	A	Actual P K	Allow. P <sub>a</sub> K	Ratio P / P <sub>a</sub>
	ft		ft	ft		ksi	in <sup>2</sup>			
T1	180 - 160	ROHN 2 STD	20.00	4.00	61.0 K=1.00	22.549	1.0745	-5.03	24.23	0.208
T2	160 - 140	ROHN 2 STD	20.00	4.00	61.0 K=1.00	22.549	1.0745	-16.28	24.23	0.672 ✓
T3	140 - 120	ROHN 2.5 STD	20.03	5.01	63.4 K=1.00	22.122	1.7040	-32.58	37.70	0.864 ✓
T4	120 - 113.334	ROHN 2.5 EH	6.68	6.68	86.7 K=1.00	17.636	2.2535	-37.07	39.74	0.933 ✓
T5	113.334 - 106.667	ROHN 2.5 EH	6.68	6.68	86.7 K=1.00	17.634	2.2535	-42.44	39.74	1.068 ✓
T6	106.667 - 100.001	ROHN 2.5 EH	6.68	6.68	86.7 K=1.00	17.634	2.2535	-48.26	39.74	1.215 ✓
T7	100.001 - 80.0007	ROHN 3 X-STR	20.03	6.68	70.5 K=1.00	20.841	3.0159	-63.82	62.86	1.015 ✓
T8	80.0007 - 60.0007	ROHN 3 EH	20.04	6.68	70.5 K=1.00	20.839	3.0159	-79.31	62.85	1.262 ✓
T9	60.0007 - 40.0007	ROHN 4 X-STR	20.03	10.02	81.4 K=1.00	18.731	4.4074	-93.30	82.56	1.130 ✓
T10	40.0007 - 20.0007	ROHN 4 X-STR	20.04	10.02	81.4 K=1.00	18.729	4.4074	-108.11	82.55	1.310 ✓
T11	20.0007 - 0	ROHN 5 STD	20.03	10.02	64.0 K=1.00	22.021	4.2999	-122.68	94.69	1.296 ✓

**Diagonal Design Data (Compression)**

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	F <sub>a</sub>	A	Actual P K	Allow. P <sub>a</sub> K	Ratio P / P <sub>a</sub>
	ft		ft	ft		ksi	in <sup>2</sup>			
T1	180 - 160	L1 1/2x1 1/2x1/8	7.65	3.57	144.8 K=1.00	7.126	0.3594	-0.88	2.56	0.344 ✓
T2	160 - 140	L1 1/2x1 1/2x1/8	7.68	3.59	145.5 K=1.00	7.055	0.3594	-1.74	2.54	0.687 ✓
T3	140 - 120	L2x2x3/16	9.70	4.72	143.8 K=1.00	7.225	0.7150	-2.28	5.17	0.441 ✓
T4	120 - 113.334	L2x2x3/16	11.12	5.49	167.1 K=1.00	5.345	0.7150	-2.64	3.82	0.690 ✓
T5	113.334 - 106.667	L2 1/2x2 1/2x3/16	11.67	5.76	139.7 K=1.00	7.653	0.9020	-2.75	6.90	0.399 ✓
T6	106.667 - 100.001	L2 1/2x2 1/2x3/16	12.24	6.04	146.5 K=1.00	6.958	0.9020	-2.52	6.28	0.401 ✓
T7	100.001 - 80.0007	L2 1/2x2 1/2x3/16	13.96	6.87	166.5 K=1.00	5.384	0.9020	-3.00	4.86	0.618 ✓
T8	80.0007 - 60.0007	L2 1/2x2 1/2x3/16	15.82	7.81	189.3 K=1.00	4.167	0.9020	-3.10	3.76	0.824 ✓

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Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	F <sub>a</sub>	A	Actual P K	Allow. P <sub>a</sub> K	Ratio P / P <sub>a</sub>
	ft		ft	ft		ksi	in <sup>2</sup>			
T9	60.0007 - 40.0007	L3x3x3/16	19.04	9.46	190.4 K=1.00	4.118	1.0900	-3.93	4.49	0.875 ✓
T10	40.0007 - 20.0007	L3x3x3/16	20.81	10.35	208.5 K=1.00	3.437	1.0900	-4.13	3.75	1.103 ✓
T11	20.0007 - 0	KL/R > 200 (C) - 194 L3 1/2x3 1/2x1/4	22.61	11.19	193.5 K=1.00	3.987	1.6900	-4.78	6.74	0.709 ✓

### Horizontal Design Data (Compression)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	F <sub>a</sub>	A	Actual P K	Allow. P <sub>a</sub> K	Ratio P / P <sub>a</sub>
	ft		ft	ft		ksi	in <sup>2</sup>			
T5	113.334 - 106.667	L3x3x3/16	9.24	8.77	176.6 K=1.00	4.788	1.0900	-0.53	5.22	0.102 ✓

### Top Girt Design Data (Compression)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	F <sub>a</sub>	A	Actual P K	Allow. P <sub>a</sub> K	Ratio P / P <sub>a</sub>
	ft		ft	ft		ksi	in <sup>2</sup>			
T1	180 - 160	L2x2x1/8	6.52	6.32	163.6 K=0.86	5.582	0.4844	-0.07	2.70	0.025 ✓
T3	140 - 120	L2x2x1/8	6.56	6.36	164.3 K=0.86	5.532	0.4844	-0.36	2.68	0.136 ✓

### Tension Checks

### Leg Design Data (Tension)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	F <sub>a</sub>	A	Actual P K	Allow. P <sub>a</sub> K	Ratio P / P <sub>a</sub>
	ft		ft	ft		ksi	in <sup>2</sup>			
T1	180 - 160	ROHN 2 STD	20.00	4.00	61.0	30.000	1.0745	4.13	32.24	0.128 ✓
T2	160 - 140	ROHN 2 STD	20.00	4.00	61.0	30.000	1.0745	14.20	32.24	0.440 ✓
T3	140 - 120	ROHN 2.5 STD	20.03	5.01	63.4	30.000	1.7040	27.17	51.12	0.531 ✓
T4	120 - 113.334	ROHN 2.5 EH	6.68	6.68	86.7	30.000	2.2535	31.08	67.61	0.460 ✓
T5	113.334 -	ROHN 2.5 EH	6.68	6.68	86.7	30.000	2.2535	35.65	67.61	0.527 ✓

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Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	F <sub>a</sub>	A	Actual P K	Allow. P <sub>a</sub> K	Ratio P / P <sub>a</sub>
	ft		ft	ft		ksi	in <sup>2</sup>			
	106.667									
T6	106.667 - 100.001	ROHN 2.5 EH	6.68	6.68	86.7	30.000	2.2535	40.51	67.61	0.599 ✓
T7	100.001 - 80.0007	ROHN 3 X-STR	20.03	6.68	70.5	30.000	3.0159	54.07	90.48	0.598 ✓
T8	80.0007 - 60.0007	ROHN 3 EH	20.04	6.68	70.5	30.000	3.0159	67.00	90.48	0.740 ✓
T9	60.0007 - 40.0007	ROHN 4 X-STR	20.03	10.02	81.4	30.000	4.4074	78.68	132.22	0.595 ✓
T10	40.0007 - 20.0007	ROHN 4 X-STR	20.04	10.02	81.4	30.000	4.4074	90.98	132.22	0.688 ✓
T11	20.0007 - 0	ROHN 5 STD	20.03	10.02	64.0	30.000	4.2999	102.92	129.00	0.798 ✓

### Diagonal Design Data (Tension)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	F <sub>a</sub>	A	Actual P K	Allow. P <sub>a</sub> K	Ratio P / P <sub>a</sub>
	ft		ft	ft		ksi	in <sup>2</sup>			
	180 - 160	L1 1/2x1 1/2x1/8	7.65	3.57	95.7	29.000	0.2656	0.88	7.70	0.115 ✓
T2	160 - 140	L1 1/2x1 1/2x1/8	7.68	3.59	96.1	29.000	0.2656	1.71	7.70	0.222 ✓
T3	140 - 120	L2x2x3/16	8.86	4.31	86.4	21.600	0.7150	2.38	15.44	0.154 ✓
T4	120 - 113.334	L2x2x3/16	11.12	5.49	109.4	21.600	0.7150	2.43	15.44	0.158 ✓
T5	113.334 - 106.667	L2 1/2x2 1/2x3/16	11.67	5.76	91.0	21.600	0.9020	2.46	19.48	0.126 ✓
T6	106.667 - 100.001	L2 1/2x2 1/2x3/16	12.24	6.04	95.3	21.600	0.9020	2.65	19.48	0.136 ✓
T7	100.001 - 80.0007	L2 1/2x2 1/2x3/16	13.38	6.58	103.6	21.600	0.9020	2.78	19.48	0.142 ✓
T8	80.0007 - 60.0007	L2 1/2x2 1/2x3/16	15.82	7.81	122.5	21.600	0.9020	3.12	19.48	0.160 ✓
T9	60.0007 - 40.0007	L3x3x3/16	19.04	9.46	122.6	21.600	1.0900	3.82	23.54	0.162 ✓
T10	40.0007 - 20.0007	L3x3x3/16	20.81	10.35	134.0	21.600	1.0900	4.15	23.54	0.176 ✓
T11	20.0007 - 0	L3 1/2x3 1/2x1/4	22.61	11.19	124.7	21.600	1.6900	4.94	36.50	0.135 ✓

### Horizontal Design Data (Tension)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	F <sub>a</sub>	A	Actual P K	Allow. P <sub>a</sub> K	Ratio P / P <sub>a</sub>
	ft		ft	ft		ksi	in <sup>2</sup>			

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		TJL

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	F <sub>a</sub>	A	Actual P K	Allow. P <sub>a</sub> K	Ratio P / P <sub>a</sub>
	ft		ft	ft		ksi	in <sup>2</sup>			
T5	113.334 - 106.667	L3x3x3/16	9.24	8.77	115.0	21.600	1.0900	0.61	23.54	0.026 ✓

**Top Girt Design Data (Tension)**

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	F <sub>a</sub>	A	Actual P K	Allow. P <sub>a</sub> K	Ratio P / P <sub>a</sub>
	ft		ft	ft		ksi	in <sup>2</sup>			
T1	180 - 160	L2x2x1/8	6.52	6.32	121.1	21.600	0.4844	0.04	10.46	0.004 ✓
T3	140 - 120	L2x2x1/8	6.56	6.36	121.9	21.600	0.4844	0.38	10.46	0.036 ✓

**Section Capacity Table**

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	SF*P <sub>allow</sub> K	% Capacity	Pass Fail
T1	180 - 160	Leg	ROHN 2 STD	3	-5.03	32.30	15.6	Pass
T2	160 - 140	Leg	ROHN 2 STD	39	-16.28	32.30	50.4	Pass
T3	140 - 120	Leg	ROHN 2.5 STD	72	-32.58	50.25	64.8	Pass
T4	120 - 113.334	Leg	ROHN 2.5 EH	102	-37.07	52.98	70.0	Pass
T5	113.334 - 106.667	Leg	ROHN 2.5 EH	111	-42.44	52.97	80.1	Pass
T6	106.667 - 100.001	Leg	ROHN 2.5 EH	123	-48.26	52.97	91.1	Pass
T7	100.001 - 80.0007	Leg	ROHN 3 X-STR	132	-63.82	83.79	76.2	Pass
T8	80.0007 - 60.0007	Leg	ROHN 3 EH	153	-79.31	83.78	94.7	Pass
T9	60.0007 - 40.0007	Leg	ROHN 4 X-STR	174	-93.30	110.05	84.8	Pass
T10	40.0007 - 20.0007	Leg	ROHN 4 X-STR	189	-108.11	110.04	98.2	Pass
T11	20.0007 - 0	Leg	ROHN 5 STD	204	-122.68	126.22	97.2	Pass
T1	180 - 160	Diagonal	L1 1/2x1 1/2x1/8	8	-0.88	3.41	25.8	Pass
T2	160 - 140	Diagonal	L1 1/2x1 1/2x1/8	41	-1.74	3.38	51.5	Pass
T3	140 - 120	Diagonal	L2x2x3/16	77	-2.28	6.89	33.1	Pass
T4	120 - 113.334	Diagonal	L2x2x3/16	107	-2.64	5.09	51.8	Pass
T5	113.334 - 106.667	Diagonal	L2 1/2x2 1/2x3/16	119	-2.75	9.20	29.9	Pass
T6	106.667 - 100.001	Diagonal	L2 1/2x2 1/2x3/16	125	-2.52	8.37	32.0 (b) 30.1	Pass
T7	100.001 - 80.0007	Diagonal	L2 1/2x2 1/2x3/16	137	-3.00	6.47	32.5 (b) 46.4	Pass
T8	80.0007 - 60.0007	Diagonal	L2 1/2x2 1/2x3/16	158	-3.10	5.01	61.8	Pass
T9	60.0007 - 40.0007	Diagonal	L3x3x3/16	179	-3.93	5.98	65.7	Pass
T10	40.0007 - 20.0007	Diagonal	L3x3x3/16	194	-4.13	4.99	82.7	Pass
T11	20.0007 - 0	Diagonal	L3 1/2x3 1/2x1/4	209	-4.78	8.98	53.2	Pass

# RISATower

**Centek Engineering Inc.**  
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	Job	11001.CO4 ~ Wolcott North	Page
	Project	180' Self-Support Lattice 1192 Wolcott Road., Wolcott, CT	Date
	Client	Verizon Wireless	Designed by TJL

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	SF*Pallow K	% Capacity	Pass Fail
T5	113.334 - 106.667	Horizontal	L3x3x3/16	112	-0.53	6.96	57.5 (b) 7.7	Pass
T1	180 - 160	Top Girt	L2x2x1/8	4	-0.07	3.60	11.0 (b) 1.8	Pass
T3	140 - 120	Top Girt	L2x2x1/8	73	-0.36	3.57	10.2	Pass
							Summary	
							Leg (T10)	98.2
							Diagonal (T10)	82.7
							Horizontal (T5)	11.0
							Top Girt (T3)	10.2
							Bolt Checks	60.3
							RATING =	98.2
								Pass
								Pass

## Element Map

Section No.	Section Elevation ft	Component Type	Element List
T1	180.00-160.00	Leg	1-3
		Diagonal	7-36
		Top Girt	4-6
T2	160.00-140.00	Leg	37-39
		Diagonal	40-69
T3	140.00-120.00	Leg	70-72
		Diagonal	76-99
		Top Girt	73-75
T4	120.00-113.33	Leg	100-102
		Diagonal	103-108
T5	113.33-106.67	Leg	109-111
		Diagonal	115-120
T6	106.67-100.00	Horizontal	112-114
		Leg	121-123
T7	100.00-80.00	Diagonal	124-129
		Leg	130-132
T8	80.00-60.00	Diagonal	133-150
		Leg	151-153
T9	60.00-40.00	Diagonal	154-171
		Leg	172-174
T10	40.00-20.00	Diagonal	175-186
		Leg	187-189
T11	20.00-0.00	Diagonal	190-201
		Leg	202-204
		Diagonal	205-216
			Total number of elements: 216



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Subject:

Anchor Bolt Analysis

Location:

Wolcott, CT

Rev. 0: 1/24/11

Prepared by: T.J.L. Checked by: C.F.C.  
Job No. 11001.CO.1

### Tower Anchor Bolt Analysis

#### Max Leg Reactions:

$$\text{Uplift} = \text{Uplift} := 106\text{-kips} \quad (\text{User Input})$$

$$\text{Shear} = \text{Shear} := 14\text{-kips} \quad (\text{User Input})$$

$$\text{Compression} = \text{Compression} := 126\text{-kips} \quad (\text{User Input})$$

#### Anchor Bolt Data:

Use ASTM A354 Gr. BC

$$\text{Number of Anchor Bolts} = N := 4 \quad (\text{User Input})$$

$$\text{Bolt Ultimate Strength} = F_u := 125\text{ksi} \quad (\text{User Input})$$

$$\text{Bolt Yield Strength} = F_y := 109\text{ksi} \quad (\text{User Input})$$

$$\text{Diameter of Bolts} = D := 1.0\text{in} \quad (\text{User Input})$$

$$\text{Threads per Inch} = n := 8 \quad (\text{User Input})$$

$$\text{Coefficient of Friction} = \mu := 0.55 \quad (\text{User Input})$$

#### Anchor Bolt Area:

$$\text{Gross Area of Bolt} = A_g := \frac{\pi}{4} \cdot D^2 = 0.785 \cdot \text{in}^2$$

$$\text{Net Area of Bolt} = A_n := \frac{\pi}{4} \left( D - \frac{0.9743 \cdot \text{in}}{n} \right)^2 = 0.606 \cdot \text{in}^2 \quad (\text{AISC 13th Ed. pg. 7-83})$$

Subject:

Anchor Bolt Analysis

Location:

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Prepared by: T.J.L. Checked by: C.F.C.  
Job No. 11001.CO.1Check Tensile Force:

Maximum Tensile Force (Gross Area) =

$$F_{gross.area} := 1.33 \cdot (0.33 \cdot A_g \cdot F_u) = 43.1\text{-kips}$$

Maximum Tensile Force (Net Area) =

$$F_{net.area} := 1.33 \cdot (0.60 \cdot A_n \cdot F_y) = 52.7\text{-kips}$$

Allowable Tension =

$$\text{AllowableTension} := \begin{cases} F_{gross.area} & \text{if } F_{gross.area} < F_{net.area} \\ F_{net.area} & \text{if } F_{net.area} < F_{gross.area} \end{cases}$$

$$\text{AllowableTension} = 43.1\text{-kips}$$

Applied Tension =

$$\text{MaxTension} := \frac{\text{Uplift}}{N} = 26.5\text{-kips}$$

$$\frac{\text{MaxTension}}{F_{net.area}} = 50.3\text{-\%}$$

$$\text{Condition1} := \text{if} \left( \frac{\text{MaxTension}}{F_{net.area}} \leq 1.00, \text{"OK"}, \text{"Overstressed"} \right)$$

Condition1 = "OK"

Check Anchor Bolt Area:

Based on the ASCE 10-97 Design of Latticed Steel Transmission Structures

Required Area =

$$A_{s1} := \frac{\text{Uplift}}{F_y} + \frac{\text{Shear}}{\mu \cdot 0.85 \cdot F_y} = 1.2\text{-in}^2$$

$$A_{s2} := \left| \frac{\text{Shear} - (0.3 \cdot \text{Compression})}{\mu \cdot 0.85 \cdot F_y} \right| = 0.467\text{-in}^2$$

Provided Area =

$$A_{provided} := A_n \cdot N = 2.4\text{-in}^2$$

$$\text{Condition2} := \text{if} \left( \frac{A_{s1}}{A_{provided}} \leq 1.00, \text{"OK"}, \text{"Overstressed"} \right)$$

Condition2 = "OK"

$$\text{Condition3} := \text{if} \left( \frac{A_{s2}}{A_{provided}} \leq 1.00, \text{"OK"}, \text{"Overstressed"} \right)$$

Condition3 = "OK"



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Subject:

FOUNDATION ANALYSIS

Location:

Wolcott, CT

Rev. 0: 1/24/11

Prepared by: T.J.L. Checked by: C.F.C.  
Job No. 11001.CO1

### Pier and Mat Foundation Analysis:

#### Input Data:

##### Tower Data:

Overspinning Moment =	$OM := 2170\text{-ft}\cdot\text{kip}$	(User Input from RISATower)
Shear Force =	$S_t := 23\text{-kip}$	(User Input from RISATower)
Axial Force =	$WT_t := 16\text{-kip}$	(User Input from RISATower)
Max Compression Force =	$C_t := 126\text{-kip}$	(User Input from RISATower)
Max Uplift Force =	$U_t := 106\text{-kip}$	(User Input from RISATower)
Tower Height =	$H_t := 180\text{-ft}$	(User Input)
Tower Width =	$W_t := 20.78\text{-ft}$	(User Input)
Tower Position on Foundation (1=offset, 2=centered) =	$Pos_t := 2$	(User Input)

##### Footing Data:

Overall Depth of Footing =	$D_f := 4.0\text{-ft}$	(User Input)
Length of Pier =	$L_p := 0\text{-ft}$	(User Input)
Extension of Pier Above Grade =	$L_{pag} := 0\text{-ft}$	(User Input)
Diameter of Pier =	$d_p := 0\text{-ft}$	(User Input)
Thickness of Footing =	$T_f := 4.0\text{-ft}$	(User Input)
Width of Footing =	$W_f := 28.5\text{-ft}$	(User Input)

##### Material Properties:

Concrete Compressive Strength =	$f_c := 3000\text{-psi}$	(User Input)
Steel Reinforcement Yield Strength =	$f_y := 60000\text{-psi}$	(User Input)
Internal Friction Angle of Soil =	$\Phi_s := 34\text{-deg}$	(User Input)
Allowable Soil Bearing Capacity =	$q_s := 3000\text{-psf}$	(User Input)
Unit Weight of Soil =	$\gamma_{soil} := 60\text{-pcf}$	(User Input)
Unit Weight of Concrete =	$\gamma_{conc} := 150\text{-pcf}$	(User Input)
Foundation Bouyancy =	$Bouyancy := 0$	(User Input) (Yes=1 / No=0)
Depth to Neglect =	$n := 0\text{-ft}$	(User Input)
Cohesion of Clay Type Soil =	$c := 0\text{-ksf}$	(User Input) (Use 0 for Sandy Soil)
Seismic Zone Factor =	$Z := 2$	(User Input) (UBC-1997 Fig 23-2)
Coefficient of Friction Between Concrete =	$\mu := 0.45$	(User Input)



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Pier Reinforcement:

Bar Size =	$BS_{pier} := 0$	(User Input)	
Bar Diameter =	$d_{bpier} := 1.0\text{-in}$	(User Input)	
Number of Bars =	$NB_{pier} := 0$	(User Input)	
Clear Cover of Reinforcement =	$Cvr_{pier} := 3\text{-in}$	(User Input)	
Reinforcement Location Factor =	$\alpha_{pier} := 1.0$	(User Input)	(ACI-2008 12.2.4)
Coating Factor =	$\beta_{pier} := 1.0$	(User Input)	(ACI-2008 12.2.4)
Concrete Strength Factor =	$\lambda_{pier} := 1.0$	(User Input)	(ACI-2008 12.2.4)
Reinforcement Size Factor =	$\gamma_{pier} := 1.0$	(User Input)	(ACI-2008 12.2.4)
Diameter of Tie =	$d_{Tie} := 4\text{-in}$	(User Input)	

Pad Reinforcement:

Bar Size =	$BS_{top} := 0$	(User Input)	(Top of Pad)
Bar Diameter =	$d_{btop} := 0\text{-in}$	(User Input)	(Top of Pad)
Number of Bars =	$NB_{top} := 0$	(User Input)	(Top of Pad)
Bar Size =	$BS_{bot} := 7$	(User Input)	(Bottom of Pad)
Bar Diameter =	$d_{bbot} := 0.875\text{-in}$	(User Input)	(Bottom of Pad)
Number of Bars =	$NB_{bot} := 29$	(User Input)	(Bottom of Pad)
Clear Cover of Reinforcement =	$Cvr_{pad} := 3.0\text{-in}$	(User Input)	
Reinforcement Location Factor =	$\alpha_{pad} := 1.0$	(User Input)	(ACI-2008 12.2.4)
Coating Factor =	$\beta_{pad} := 1.0$	(User Input)	(ACI-2008 12.2.4)
Concrete Strength Factor =	$\lambda_{pad} := 1.0$	(User Input)	(ACI-2008 12.2.4)
Reinforcement Size Factor =	$\gamma_{pad} := 1.0$	(User Input)	(ACI-2008 12.2.4)

**Calculated Factors:**

Pier Reinforcement Bar Area =	$A_{bpier} := \frac{\pi \cdot d_{bpier}^2}{4} = 0.785\text{-in}^2$
Pad Top Reinforcement Bar Area =	$A_{btop} := \frac{\pi \cdot d_{btop}^2}{4} = 0\text{-in}^2$
Pad Bottom Reinforcement Bar Area =	$A_{bbot} := \frac{\pi \cdot d_{bbot}^2}{4} = 0.601\text{-in}^2$
Coefficient of Lateral Soil Pressure =	$K_p := \frac{1 + \sin(\Phi_s)}{1 - \sin(\Phi_s)} = 3.537$
Load Factor =	$LF := \begin{cases} 1.333 & \text{if } H_t \leq 700\text{-ft} \\ 1.7 & \text{if } H_t \geq 1200\text{-ft} \\ 1.333 + \left( \frac{H_t - 700\text{ft}}{1200\text{ft} - 700\text{ft}} \right) \cdot 0.4 & \text{otherwise} \end{cases} = 1.333$

**Stability of Footing:**

Adjusted Concrete Unit Weight =

$$\gamma_c := \text{if}(\text{Bouyancy} = 1, \gamma_{conc} - 62.4\text{pcf}, \gamma_{conc}) = 150\text{-pcf}$$

Adjusted Soil Unit Weight =

$$\gamma_s := \text{if}(\text{Bouyancy} = 1, \gamma_{soil} - 62.4\text{pcf}, \gamma_{soil}) = 60\text{-pcf}$$

Passive Pressure =

$$P_{pn} := K_p \cdot \gamma_s \cdot n + c \cdot 2 \cdot \sqrt{K_p} = 0\text{-ksf}$$

$$P_{pt} := K_p \cdot \gamma_s \cdot (D_f - T_f) + c \cdot 2 \cdot \sqrt{K_p} = 0\text{-ksf}$$

$$P_{top} := \text{if}[n < (D_f - T_f), P_{pt}, P_{pn}] = 0\text{-ksf}$$

$$P_{bot} := K_p \cdot \gamma_s \cdot D_f + c \cdot 2 \cdot \sqrt{K_p} = 0.849\text{-ksf}$$

$$P_{ave} := \frac{P_{top} + P_{bot}}{2} = 0.424\text{-ksf}$$

$$T_p := \text{if}[n < (D_f - T_f), T_f, (D_f - n)] = 4$$

$$A_p := W_f \cdot T_p = 114$$

Ultimate Shear =

$$S_u := P_{ave} \cdot A_p = 48.388\text{-kip}$$

Weight of Concrete =

$$WT_c := \left[ \left( W_f^2 \cdot T_f \right) + (3) \cdot \left( \frac{d_p^2 \cdot \pi}{4} L_p \right) \right] \cdot \gamma_c = 487.35\text{-kip}$$

Weight of Soil Above Footing =

$$WT_{s1} := \left[ \left( W_f^2 - (3) \cdot \left( \frac{d_p^2 \cdot \pi}{4} \right) \right) \cdot (|L_p - L_{pag} - n|) \right] \cdot \gamma_s = 0\text{-kip}$$

Weight of Soil Wedge at Back Face =

$$WT_{s2} := \left[ \frac{(L_p - L_{pag})^2 \cdot \tan(\Phi_s)}{2} \cdot W_f \right] \cdot \gamma_s = 0\text{-kip}$$

Tower Offset =

$$X_{t1} := \left[ \frac{W_f}{2} - \frac{(W_t \cdot \cos(30\text{-deg}))}{2} \right] \quad X_{t2} := \frac{W_f}{2} - \frac{(W_t \cdot \cos(30\text{-deg}))}{3}$$

$$X_t := \text{if}(Pos_t = 1, X_{t1}, X_{t2}) = 8.251$$

$$X_{off1} := \frac{W_f}{2} - \left[ \frac{(W_t \cdot \cos(30\text{-deg}))}{3} + X_t \right] = 0 \quad X_{off2} := 0$$

$$X_{off} := \text{if}(Pos_t = 1, X_{off1}, X_{off2}) = 0$$

Total Weight =

$$WT_{tot} := WT_c + WT_{s1} = 487.3\text{-kip}$$

Resisting Moment =

$$M_r := (WT_{tot}) \cdot \frac{W_f}{2} + S_u \cdot \frac{T_f}{3} + WT_{s2} \left[ W_f + \frac{(L_p - L_{pag}) \cdot \tan(\Phi_s)}{3} \right] = 7009\text{-kip}\cdot\text{ft}$$

Overturning Moment =

$$M_{ot} := OM + S_t \cdot (L_p + T_f) = 2262\text{-kip}\cdot\text{ft}$$

Factor of Safety Actual =

$$FS := \frac{M_r}{M_{ot}} = 3.1$$

Factor of Safety Required =

$$FS_{req} := 2$$

Overturning\_Moment\_Check := if(FS ≥ FS\_req, "Okay", "No Good")

Overturning\_Moment\_Check = "Okay"

**Bearing Pressure Caused by Footing:**

Total Load =

$$\text{Load}_{\text{tot}} := \text{WT}_c + \text{WT}_{s1} + \text{WT}_t = 503\text{-kip}$$

Area of the Mat =

$$A_{\text{mat}} := W_f^2 = 812.25$$

Section Modulus of Mat =

$$S := \frac{W_f^3}{6} = 3858.19\text{-ft}^3$$

Maximum Pressure in Mat =

$$P_{\text{max}} := \frac{\text{Load}_{\text{tot}}}{A_{\text{mat}}} + \frac{M_{\text{ot}}}{S} = 1.206\text{-ksf}$$

$$\text{Max\_Pressure\_Check} := \text{if}(P_{\text{max}} < q_s, \text{"Okay"}, \text{"No Good"})$$

Max\_Pressure\_Check = "Okay"

Minimum Pressure in Mat =

$$P_{\text{min}} := \frac{\text{Load}_{\text{tot}}}{A_{\text{mat}}} - \frac{M_{\text{ot}}}{S} = 0.033\text{-ksf}$$

$$\text{Min\_Pressure\_Check} := \text{if}\left[\left(P_{\text{min}} \geq 0\right) \cdot \left(P_{\text{min}} < q_s\right), \text{"Okay"}, \text{"No Good"}\right]$$

Min\_Pressure\_Check = "Okay"

Distance to Resultant of Pressure Distribution =

$$X_p := \frac{P_{\text{max}}}{P_{\text{max}} - P_{\text{min}}} \cdot \frac{1}{3} = 9.771$$

$$X_k := \frac{W_f}{6} = 4.75$$

Since Resultant Force is Not in Kern, Area to which Pressure is Applied Must be Reduced.

Eccentricity =

$$e := \frac{M_{\text{ot}}}{\text{WT}_{\text{tot}}} = 4.641$$

Adjusted Soil Pressure =

$$P_a := \frac{2 \cdot \text{WT}_{\text{tot}}}{3 \cdot W_f \left( \frac{W_f}{2} - e \right)} = 1.186\text{-ksf}$$

$$q_{\text{adj}} := \text{if}(P_{\text{min}} < 0, P_a, P_{\text{max}}) = 1.206\text{-ksf}$$

$$\text{Pressure\_Check} := \text{if}(q_{\text{adj}} < q_s, \text{"Okay"}, \text{"No Good"})$$

Pressure\_Check = "Okay"

**Shear Strength of Concrete:**Beam Shear:(Critical section located at a distance d from  
the face of Pier)

(ACI 11.3.1.1)

$$\phi_c := 0.85$$

(ACI 9.3.2.5)

$$d := T_f - C_{v, \text{pad}} - d_{\text{bot}} = 44.125 \text{-in}$$

$$FL := LF \cdot \frac{C_t}{W_f^2} = 0.207 \cdot \text{ksf}$$

$$V_{\text{req}} := FL \cdot (X_t - 0.5 \cdot d_p - d) \cdot W_f = 26.957 \cdot \text{kips}$$

$$V_{\text{Avail}} := \phi_c \cdot 2 \cdot \sqrt{f_c \cdot \psi} \cdot W_f \cdot d = 1405 \cdot \text{kip} \quad (\text{ACI-2008 11.2.1.1})$$

$$\text{Beam\_Shear\_Check} := \text{if}(V_{\text{req}} < V_{\text{Avail}}, \text{"Okay"}, \text{"No Good"})$$

Beam\_Shear\_Check = "Okay"

Punching Shear:(Critical Section Located at a distance of d/2  
from the face of pier)

(ACI 11.11.1.2)

$$\text{Critical Perimeter of Punching Shear} =$$

$$b_o := (d_p + d) \cdot \pi = 11.6$$

$$\text{Area Included Inside Perimeter} =$$

$$A_{bo} := \frac{\pi \cdot (d_p + d)^2}{4} = 10.6$$

$$\text{Required Shear Strength} =$$

$$V_{\text{req}} := FL \cdot (W_f^2 - A_{bo}) = 166 \cdot \text{kips}$$

$$\text{Available Shear Strength} =$$

$$V_{\text{Avail}} := \phi_c \cdot 4 \cdot \sqrt{f_c \cdot \psi} \cdot b_o \cdot d = 1139.1 \cdot \text{kip} \quad (\text{ACI-2008 11.11.2.1})$$

$$\text{Punching\_Shear\_Check} := \text{if}(V_{\text{req}} < V_{\text{Avail}}, \text{"Okay"}, \text{"No Good"})$$

Punching\_Shear\_Check = "Okay"



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Subject:

FOUNDATION ANALYSIS

Location:

Wolcott, CT

Rev. 0: 1/24/11

Prepared by: T.J.L. Checked by: C.F.C.  
Job No. 11001.CO1

### Steel Reinforcement in Pad:

#### Required Reinforcement for Bending:

$$\text{Strength Reduction Factor} = \phi_m := .90 \quad (\text{ACI-2008 9.3.2.1})$$

$$M_{nT} := LF \left[ U_t \left( W_t \cdot \sin(60\text{-deg}) - \frac{d_p}{2} \right) + S_t (D_f + L_{pag}) \right] - W T_t X_{off} = 3 \times 10^6 \text{ lbf}$$

$$M_{nS} := -1 \cdot \left[ \frac{1}{2} \cdot \left( \frac{W_f}{2} + \frac{W_t}{3} \cdot \cos(30\text{-deg}) - \frac{d_p}{2} \right)^2 \cdot W_t \cdot [\gamma_s (T_f - T_f)] + W T_s 2 \cdot \left[ \frac{W_f}{2} + \frac{W_t}{3} \cdot \cos(30\text{-deg}) - \frac{d_p}{2} + (D_f - n) \cdot \tan(\Phi_s) \right] \right]$$

$$M_{nC} := -1 \cdot \left[ \frac{1}{2} \cdot \left( \frac{W_f}{2} + \frac{W_t}{3} \cdot \cos(30\text{-deg}) - \frac{d_p}{2} \right)^2 \cdot W_t \cdot (\gamma_c \cdot T_f) \right]$$

$$\text{Design Moment} = M_n := \frac{M_{nT} + M_{nS} + M_{nC}}{\phi_m} = 121.603 \text{ kips}\cdot\text{ft}$$

$$\beta := \begin{cases} 0.85 & \text{if } 2500 \text{-psi} \leq f_c \leq 4000 \text{-psi} \\ 0.65 & \text{if } f_c > 8000 \text{-psi} \\ \left[ 0.85 - \left[ \frac{(f_c - 4000)}{1000} \right] \cdot 0.5 \right] & \text{otherwise} \end{cases} = 0.85 \quad (\text{ACI-2008 10.2.7.3})$$

$$b_{eff} := W_t \cdot \cos(30\text{-deg}) + d_p = 215.952 \text{ in}$$

$$A_s := \frac{M_n}{(f_y d)} = 0.551 \cdot \text{in}^2$$

$$a := \frac{A_s \cdot f_y}{\beta \cdot f_c \cdot b_{eff}} = 0.06 \text{ in}$$

$$A_s := \frac{M_n}{f_y \left( d - \frac{a}{2} \right)} = 0.552 \cdot \text{in}^2$$

$$\rho := \frac{A_s}{b_{eff} d} = 0.00069 \text{ in}$$

Required Reinforcement for Temperature and Shrinkage:

$$\rho_{sh} := \begin{cases} 0.0018 & \text{if } f_y \geq 60000 \cdot \text{psi} \\ 0.0020 & \text{otherwise} \end{cases} = 0.0018 \quad (\text{ACI -2008 7.12.2.1})$$

Check Bottom Bars:

$$As := \text{if} \left( \rho \geq \rho_{sh}, A_s, \rho_{sh} \cdot \frac{b_{eff}}{2} \cdot d \right) = 8.6 \cdot \text{in}^2$$

$$As_{prov} := A_{bbot} \cdot NB_{bot} = 17.4 \cdot \text{in}^2$$

$$\text{Pad_Reinforcement_Bot} := \text{if}(As_{prov} > As, \text{"Okay"}, \text{"No Good"})$$

Pad\_Reinforcement\_Bot = "Okay"

**Developement Length Pad Reinforcement:**

Bar Spacing =

$$B_{sPad} := \frac{W_f - 2 \cdot Cvr_{pad} - NB_{bot} \cdot d_{bbot}}{NB_{bot} - 1} = 11.09 \cdot \text{in}$$

Spacing or Cover Dimension =

$$c := \text{if} \left( Cvr_{pad} < \frac{B_{sPad}}{2}, Cvr_{pad}, \frac{B_{sPad}}{2} \right) = 3 \cdot \text{in}$$

Transverse Reinforcement Index =

$$k_{tr} := 0 \quad (\text{ACI-2008 12.2.3})$$

$$L_{dbt} := \frac{3 \cdot f_y \alpha_{pad} \beta_{pad} \gamma_{pad} \lambda_{pad}}{40 \cdot \sqrt{f_c \cdot \text{psi}}} \cdot \frac{c + k_{tr}}{d_{bbot}} \cdot d_{bbot} = 21 \cdot \text{in}$$

Minimum Development Length =

$$L_{dbmin} := 12 \cdot \text{in} \quad (\text{ACI-2008 12.2.1})$$

$$L_{dbtCheck} := \text{if}(L_{dbt} \geq L_{dbmin}, \text{"Use L.dbt"}, \text{"Use L.dbmin"}) = \text{"Use L.dbt"}$$

Available Length in Pad =

$$L_{Pad} := \frac{W_f}{2} - \frac{W_t}{2} - Cvr_{pad} = 43.32 \cdot \text{in}$$

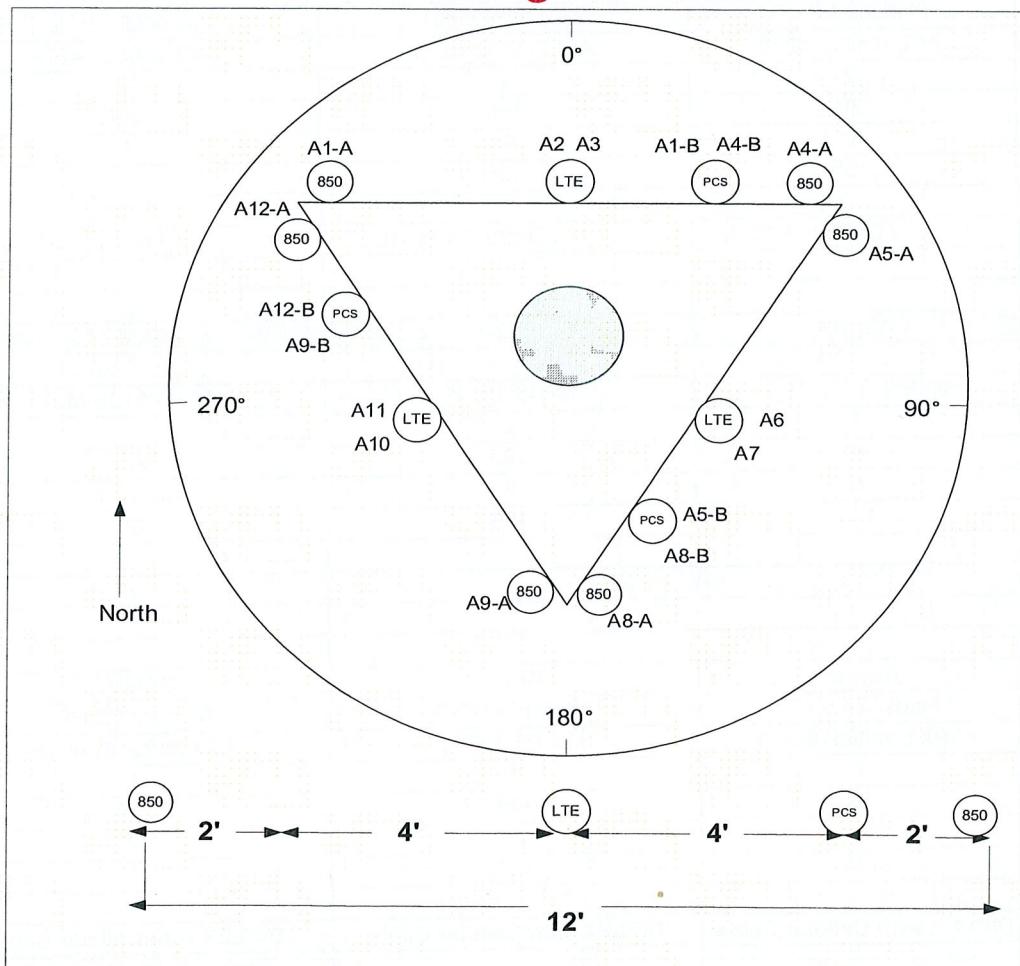
$$L_{pad\_Check} := \text{if}(L_{Pad} > L_{dbt}, \text{"Okay"}, \text{"No Good"})$$

L\_{pad\\_Check} = "Okay"

SITE NAME	WOLCOTT N CT		ECP - CELL #	2	343		
LATITUDE	41-37-05.37 N		LONGITUDE	72-58-14.38 W			
Additional Comments:			SAVE BUTTON				
			STRUCTURE TYPE	LATTICE			
700 Mhz - LTE ANTENNA ADD	ALPHA	BETA	GAMMA				
EQUIPMENT TYPE	eNodeB	eNodeB	eNodeB				
ANTENNA TYPE	BXA-70063-6CF 4°		BXA-70063-6CF 4°		BXA-70063-6CF 4°		
QTY OF ANTENNAS PER FACE	1	1	1				
ORIENTATION (DEG)	20	180	280				
DOWN TILT ( MECH/DEG )	0°	3°	0°				
RAD CTR (FT AGL)	135	135	135				
TMA - QTY / MODEL							
DIPLEXER - QTY / MODEL							
MCPA BRICKS (QTY)							
850 Cellular - Current Config	ALPHA	BETA	GAMMA				
EQUIPMENT TYPE	Modcell 4.0 HD	Modcell 4.0 HD	Modcell 4.0 HD				
ANTENNA TYPE	WPA-80063-4CF		WPA-80080/4CF		WPA-80063-4CF		
QTY OF ANTENNAS PER FACE	2	2	2				
ORIENTATION (DEG)	20	195	290				
DOWN TILT ( MECH/DEG )	10	4	2				
RAD CTR (FT AGL)	135	135	135				
TMA - QTY / MODEL							
DIPLEXER - QTY / MODEL							
DIPLEXER KIT - QTY / MODEL							
MCPA BRICKS (QTY)							
850 Cellular - Future Config	ALPHA	BETA	GAMMA				
EQUIPMENT TYPE	Modcell 4.0 HD	Modcell 4.0 HD	Modcell 4.0 HD				
ANTENNA TYPE	APL868013-42T0		APL868013-42T0		APL866513-42T0		
QTY OF ANTENNAS PER FACE	2	2	2				
ORIENTATION (DEG)	20	180	280				
DOWN TILT ( MECH/DEG )	4°	6°	4°				
RAD CTR (FT AGL)	135	135	135				
TMA - QTY / MODEL							
DIPLEXER - QTY / MODEL	2	FD9R6004/2C-3L	2	FD9R6004/2C-3L	2		
DIPLEXER KIT - QTY / MODEL							
MCPA BRICKS (QTY)							
1900 PCS - Current Config	ALPHA	BETA	GAMMA				
EQUIPMENT TYPE	Modcell 4.0 HD	Modcell 4.0 HD	Modcell 4.0 HD				
ANTENNA TYPE	950F65T2ZE-M_2		948F85T2E-M_2		948F85T2E-M_2		
QTY OF ANTENNAS PER FACE	2	2	2				
ORIENTATION (DEG)	20	195	290				
DOWN TILT ( MECH/DEG )	0	2	0				
RAD CTR (FT AGL)	135	135	135				
TMA - QTY / MODEL							
DIPLEXER - QTY / MODEL							
DIPLEXER KIT - QTY / MODEL							
MCPA BRICKS (QTY)							
1900 PCS - Future Config	ALPHA	BETA	GAMMA				
EQUIPMENT TYPE	Modcell 4.0 HD	Modcell 4.0 HD	Modcell 4.0 HD				
ANTENNA TYPE	APX18-206516L-T0		MG D3-800T0		APX18-206516L-T0		
QTY OF ANTENNAS PER FACE	1	1	1				
ORIENTATION (DEG)	20	180	280				
DOWN TILT ( MECH/DEG )	2°	3°	3°				
RAD CTR (FT AGL)	135	135	135				
TMA - QTY / MODEL							
DIPLEX WITH CELLULAR CABLE	DIPLEX with Cellular Cable		DIPLEX with Cellular Cable		DIPLEX with Cellular Cable		
MCPA BRICKS (QTY)							

NUMBER OF CABLE'S NEEDED				ESTIMATED CABLE LENGTH			
MAINLINE SIZE	1 5/8"	TOTAL # OF MAINLINES	12	MAINLINE (FT)			
JUMPER SIZE	1/2 "	TOTAL # OF TOP JUMPERS	18	TOP JUMPER (FT)			
Equipment Cable Ordering	MAIN CABLE	12	+	TOP JUMPER #	12	+	6
TX / RX FREQUENCIES				TX POWER OUTPUT			
Cellular A-Band		PCS F-Band	700 Mhz C - E	Cellular (Watts)	20		
TX - 869-880,890-891.5 MHz		TX - 1970-1975	TX - 746-757	PCS (Watts)	16		
RX - 824-835,845-846.5 MHz		RX - 1890-1895	RX - 776-787	LTE (Watts)	40		
ALPHA		BETA	GAMMA				
Ant.	Freq.	Func.	Color Code	Ant.	Freq.	Func.	Color Code
A1-A	800	Tx1/Rx0	RED	A5-A	800	Tx2/Rx0	BLUE
A1-B	1900	Tx1/Rx0	RED/ WHITE	A5-B	1900	Tx2/Rx0	BLUE/ WHITE
A2	700	Tx1/Rx0	RED/ ORANGE	A6	700	Tx2/Rx0	BLUE/ ORANGE
A3	700	Tx4/Rx1	RED/RED/ ORANGE	A7	700	Tx5/Rx1	BLUE/BLUE/ ORANGE
A4-B	1900	Tx4/Rx1	RED/RED/ WHITE	A8-B	1900	Tx5/Rx1	BLUE/BLUE/ WHITE
A4-A	800	Tx4/Rx1	RED/RED	A8-A	800	Tx5/Rx1	BLUE/BLUE
RF ENGINEER				RF MANAGER			
Prepared By : Dany Bustamante				INITIALS			
Steve Weatherbee				DB			
				1/25/2011			

## Site Configuration



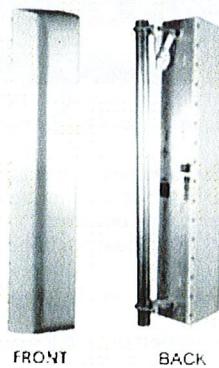
## Maximizer® Log Periodic Antenna, 806-894, 65deg, 15.1dBi, 1.2m, FET, 0deg

**Product Description**

The Celwave® Maximizer series is a log periodic dipole array which uses a patented design to achieve a front-to-back ratio of 45 dB, the highest front-to-back ratio in the industry. Maximizers are available to cover ESMR, AMPS, PCS and DCS frequency ranges. They use RFS's patented monolithic CELlite® technology, which eliminates cable and soldered joints to reduce the possibility of inter-modulation products. The CELlite technology assures high reliability and excellent repeatability of electrical characteristics. The cellular Maximizers are available in 65°, 80° and 90° horizontal beamwidths and the PCS/DCS Maximizers are available in 65° and 90° horizontal beamwidths. Patent number 6,133,889.

**Features/Benefits**

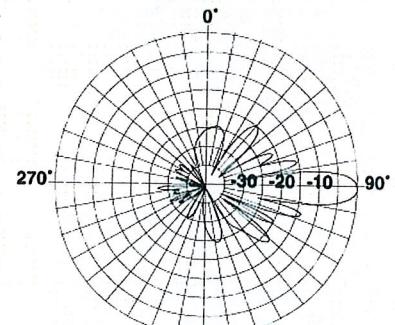
- 45 dB front-to-back ratio reduces co-channel interference.
- Monolithic construction reduces IM.
- No solder joints, high reliability.
- Surface treated components prevent galvanic corrosion.
- UV stabilized radome assures long life without radome deterioration due to UV exposure.



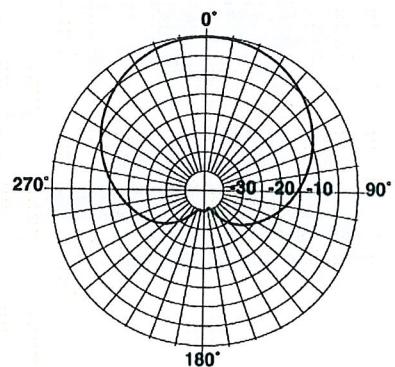
FRONT BACK

**Technical Specifications****Electrical Specifications**

Frequency Range, MHz	806-894
Horizontal Beamwidth, deg	65
Vertical Beamwidth, deg	15
Electrical Downtilt, deg	0
Gain, dBi (dBd)	15.1 (13)
1st Upper Sidelobe Suppression, dB	>20
Upper Sidelobe Suppression, dB	>20
Front-To-Back Ratio, dB	45
Polarization	Vertical
VSWR	< 1.5:1
Impedance, Ohms	50
Maximum Power Input, W	500
Lightning Protection	Direct Ground
Connector Type	7-16 DIN Female



Vertical Pattern



Horizontal Pattern

**Ordering Information**

Mounting Hardware	APM21-3
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**Other Documentation**

Optimizer® Dual Polarized Antenna, 1710-2170, 65deg, 17.6/18.6dBi, 1.3m, FET, 0deg

**Product Description**

Dense urban networks where site aspect is essential.

**Features/Benefits**

- Very broadband design operating from GSM1800 up to 3G-UMTS.
- Reduction of visual impact by gathering 3 antennas in a cylindrical volume.
- Reduction of site dimensions will ease site acceptance.
- Possible camouflage solution on demand.
- Wind load thrust highly reduced.
- Compatible with usual base stations with 35 dB typical isolation between ports.
- Effective polarization diversity ensured by high cross polar discrimination.
- Optimized suppression of side lobes allows strong mechanical tilt.

**Technical Specifications****Electrical Specifications**

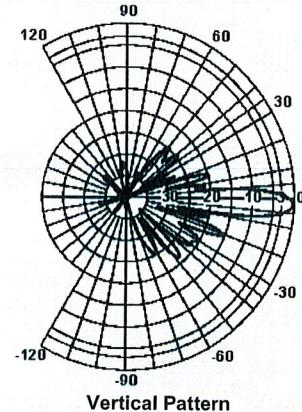
Frequency Range, MHz	1710-1900	1900-2170
Horizontal Beamwidth, deg	69	64
Vertical Beamwidth, deg	6.9	6
Electrical Downtilt, deg	0	
Gain, dBi (dBd)	17.6 (15.5)	18.6 (16.5)
1st Upper Sidelobe Suppression, dB	>20	
Front-To-Back Ratio, dB	>29	30
Polarization	Dual pol +/-45°	
VSWR	< 1.4:1	
Isolation between Ports, dB	>30 (typ 35)	
3rd Order IMP @ 2 x 43 dBm, dBc	>150, N/A	
7th Order IMP @ 2 x 46 dBm, dBc	N/A, >170	
Impedance, Ohms	50	
Maximum Power Input, W	300	
Lightning Protection	Direct Ground	
Connector Type	(2) 7-16 Long Neck Female	

**Mechanical Specifications**

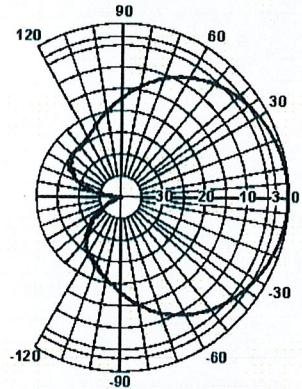
Dimensions - HxWxD, mm (in)	1349 x 169 x 80 (53.0 x 6.65 x 3.15)
Weight w/o Mtg Hardware, kg (lb)	8.5 (18.7)
Survival Wind Speed, km/h (mph)	200 (125)
Rated Wind Speed, km/h (mph)	160 (100)
Max Wind Loading Area, m² (ft²)	0.23 (2.46)
Front Thrust @ Rated Wind, N (lbf)	406 (91)
Maximum Thrust @ Rated Wind, N (lbf)	406 (91)
Wind Load - Side @ Rated Wind, N (lbf)	236 (53)
Wind Load - Rear @ Rated Wind, N (lbf)	196 (44)
Radome Material	Fiberglass
Radome Color	Light Grey RAL7035
Mounting Hardware Material	Diecasted Aluminum
Shipping Weight, kg (lb)	13.5 (30)
Packing Dimensions, HxWxD, mm (in)	1464 x 251 x 203 (57.64 x 9.88 x 7.99)

**Ordering Information**

Mounting Hardware	APM40-2
Mounting Pipe Diameter, mm (in)	60-120 (2.36-4.72)
Mounting Hardware Weight, kg (lb)	3.4 (7.5)



Vertical Pattern



Horizontal Pattern

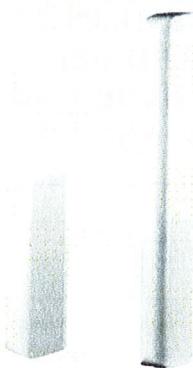
**Other Documentation**

[APM40 Series Datasheet](#)  
[APM40 Series Installation Instructions](#)

## Maximizer® Log Periodic Antenna, 806-894, 80deg, 14.1dBi, 1.2m, FET, 0deg

**Product Description**

The Celwave® Maximizer series is a log periodic dipole array which uses a patented design to achieve a front-to-back ratio of 45 dB, the highest front-to-back ratio in the industry. Maximizers are available to cover ESMR, AMPS, PCS and DCS frequency ranges. They use RFS's patented monolithic CELlite® technology, which eliminates cable and soldered joints to reduce the possibility of inter-modulation products. The CELlite technology assures high reliability and excellent repeatability of electrical characteristics. The cellular Maximizers are available in 65°, 80° and 90° horizontal beamwidths and the PCS/DCS Maximizers are available in 65° and 90° horizontal beamwidths. Patent number 6,133,889.

**Features/Benefits**

- 45 dB front-to-back ratio reduces co-channel interference.
- Monolithic construction reduces IM.
- No solder joints, high reliability.
- Surface treated components prevent galvanic corrosion.
- UV stabilized radome assures long life without radome deterioration due to UV exposure.

**Technical Specifications****Electrical Specifications**

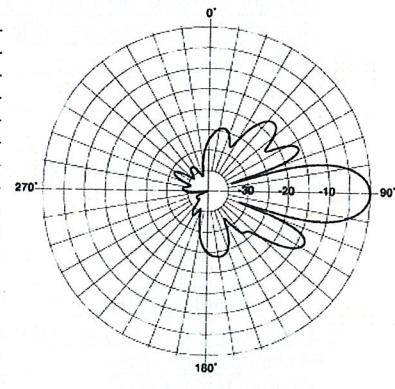
Frequency Range, MHz	806-894
Horizontal Beamwidth, deg	80
Vertical Beamwidth, deg	15
Electrical Downtilt, deg	0
Gain, dBi (dBd)	14.1 (12)
Front-To-Back Ratio, dB	45
Polarization	Vertical
VSWR	< 1.5:1
Impedance, Ohms	50
Maximum Power Input, W	500
Lightning Protection	Direct Ground
Connector Type	7-16 DIN Female

**Mechanical Specifications**

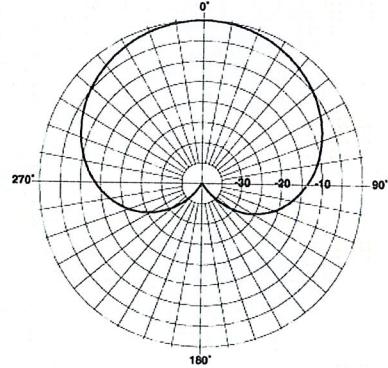
Dimensions - HxWxD, mm (in)	1219 x 152 x 203 (48 x 6 x 8)
Weight w/o Mtg Hardware, kg (lb)	2.8 (6.32)
Survival Wind Speed, km/h (mph)	200 (125)
Rated Wind Speed, km/h (mph)	200 (125)
Max Wind Loading Area, m² (ft²)	0.307 (3.3)
Maximum Thrust @ Rated Wind, N (lbf)	916 (206)
Wind Load - Side @ Rated Wind, N (lbf)	743 (167)
Radome Material	UV Stabilized High Impact ABS
Shipping Weight, kg (lb)	7.9 (17.5)
Packing Dimensions, HxWxD, mm (in)	1270 x 305 x 203 (50 x 12 x 8)

**Ordering Information**

Mounting Hardware	APM21-3
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Vertical Pattern



Horizontal Pattern

**Other Documentation**



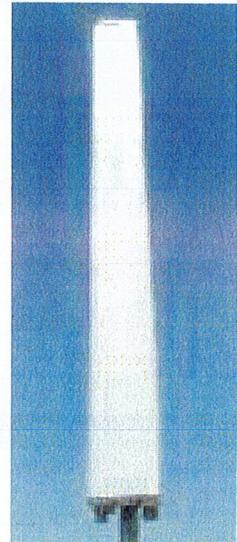
## MG D3-800Tx

**Xpol GSM1800+PCS & UMTS Panel Antenna**

**15.9 dBd/18 dBi**

**WIDE BAND 1710-2170 MHz**

**H 65° V 6.5°**



### Electrical Specifications

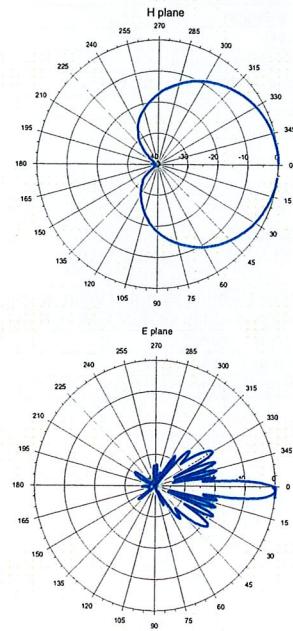
Antenna Model	MG D3-800Tx		
Frequency Range (MHz)	1710-1880	1850-1990	1920-2170
Impedance	50 Ohms		
VSWR	1.40:1		
Polarization	±45°		
Isolation between Ports (dB)	30		
Average Gain (dBd/dBi)	15.7/17.8	15.9/18	16.15/18.25
Horizontal Beamwidth (deg)	65°±5°		
Vertical Beamwidth (deg)	6.5°±0.5°	6.3°±0.5°	6.3°±0.5°
Electrical Tilt (deg)	Fixed 0°-14°		
Sidelobe Suppression (dB)	18	18	18
Front to Back Ratio (dB) @180°±20°	30		
Polarization Isolation (dB) @3 dB	20		
Beamwidth	20		
Maximum Power per Input (w)	250		
Intermodulation Products (dBc)	-150		
Connectors	2 x 7/16 Female		
Connector Position	Antenna Bottom		

### Mechanical & Environmental Specifications

Dimensions (mm)	1380 x 160 x 90
Survival Wind Speed	200 km/h
Front Windload (N) @ 160 km/h	335
Lateral Windload (N) @ 160 km/h	188
Antenna Weight (kg)	7
Clamps Weight (kg)	2
Mast Mounting	50 to 135 mm
Radome Color	Grey
Grounding	All metallic parts are DC grounded
Temperature Range	-55 to +60°C
Humidity	100 %

### Shipping Specifications

Dimensions (mm)	1580 x 340 x 210
Weight (kg)	12
Material	Cardboard and Foam



Ctra. Campo Real, Km 2,100  
28500 Arganda del Rey  
Madrid-Spain



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Fax: 34 91 876 07 09

E-mail: [telecom.commercial@rymsa.com](mailto:telecom.commercial@rymsa.com)

Web: [www.rymsa.com](http://www.rymsa.com)

## Mechanical specifications

Length	1804 mm	71.0 in
Width	285 mm	11.2 in
Depth	114 mm	4.5 in
Depth with z-bracket	154 mm	6.1 in
Weight 4)	7.9 kg	17.0 lbs
Wind Area Fore/Aft	0.51 m <sup>2</sup>	5.5 ft <sup>2</sup>
Wind Area Side	0.21 m <sup>2</sup>	2.2 ft <sup>2</sup>
Max Wind Survivability	>201 km/hr	>125 mph
Wind Load @ 100 mph (161 km/hr)		
Fore/Aft	753 N	169 lbf
Side	351 N	79 lbf

Antenna consisting of aluminum alloy with brass feedlines covered by a UV safe fiber-glass radome.

## Mounting & Downtilting

Mounting hardware attaches to pipe diameter Ø50-160 mm; Ø2.0-6.3 in

Mounting Bracket Kit	36210002
Downtilt Bracket Kit	36114003

## Electrical specifications

Frequency Range	696-900 MHz
Impedance	50Ω
Connector 3)	NE or E-DIN Female 2 ports / Center
VSWR 1)	≤ 1.35:1
Polarization	Slant ±45°
Isolation Between Ports 1)	< -25 dB
Gain 1)	14.5 dBd 16.5 dBi
Power Rating 2)	500 W
Half Power Angle 1)	
Horizontal Beamwidth	63°
Vertical Beamwidth	11°
Electrical downtilt 5)	0°
Null fill 1)	5%
Lightning protection	Direct ground

Patented Dipole Design: U.S. Patent No. 6,608,600 B2

1) Typical values.

2) Power rating limited by connector only.

3) NE indicates an elongated N connector.

E-DIN indicates an elongated DIN connector.

4) Antenna weight does not include brackets.

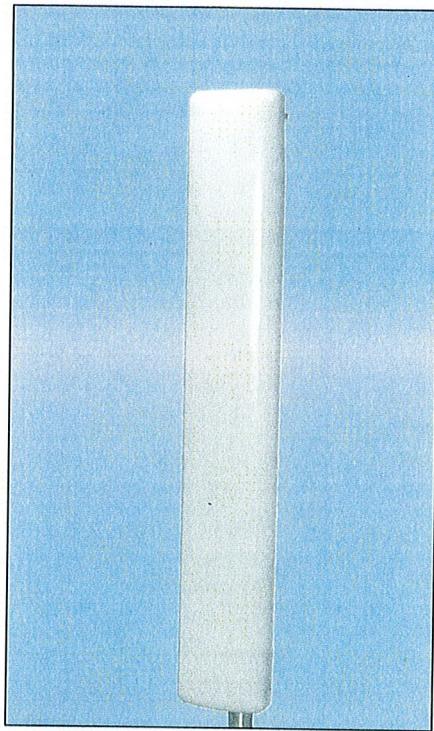
5) Add'l downtilts may be available. Check website for details.

Improvements to mechanical and/or electrical performance of the antenna may be made without notice.

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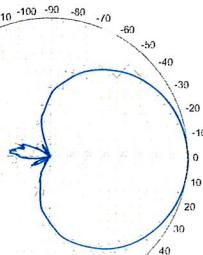
## BXA-70063/6CF

When ordering replace "—" with connector type.

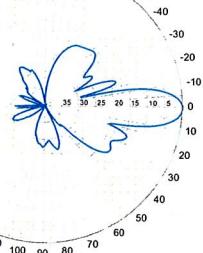


Radiation-pattern<sup>1)</sup>

750 MHz

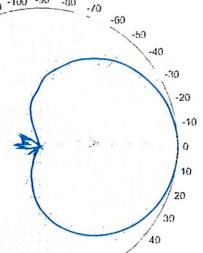


Horizontal

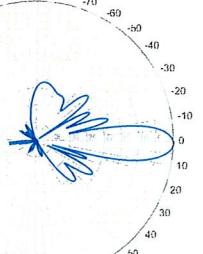


Vertical

850 MHz



Horizontal



Vertical

696-900 MHz



Featuring our Exclusive  
3T Technology™  
Antenna Design:

- Watercut brass feedline assembly for consistent performance.
- Unique feedline design eliminates the need for conventional solder joints in the signal path.
- A non-collinear system with access to every radiating element for broad bandwidth and superior performance.
- Air as insulation for virtually no internal signal loss.

### Warranty:

This antenna is under a five-year limited warranty for repair or replacement.

Revision Date: 01/08/09